Special Meeting Agenda Tolland Inland Wetlands Commission REMOTE ONLY

Thursday, December 21, 2023 at 7:00 p.m.

- 1. Call to Order
- 2. Seating of Alternate(s)
- 3. Public Participation Issues of concern not on the Agenda (2 minute limit)
- 4. Old Business
 - 4.1 <u>IWC 23-6 343 Plains Road –</u> Proposed improvements to existing Camp Yankee Trails. Regulated activity within the 200' upland review area is 1.10 acres/48,024sqft and regulated activity within the 50 feet of a wetland is 0.09 acres/48,024sqft. Zone: Residential Design District (RDD) Applicant: Girl Scouts of Connecticut.
- 5. Adjournment

To join the Zoom Meeting, either click: <u>https://us02web.zoom.us/j/8608713602?pwd=cXZLNG9SWV1vNkNjZU9NYUxCd2xiUT09</u> **One tap mobile:** +16469313860,,8608713602#,,,,*06084# Or call: 1-929-205-6099 and input: Meeting ID: 860 871 3602 Passcode: 06084



Town of Tolland Inland Wetlands Commission Г

APPLICATION FOR PERMIT

C	DEFICE USE	ONLY
Agent Decision	\$	
Commission Approval	\$	
Other	\$	

An incomplete application may be denied.

1. Applicant & Owner Information

343 Plains Road				
Site Address of Proposed Activity				
Girl Scouts of Connecticut	340 Washington St. Harford, CT 06106			
Applicant Name	Mailing Address			
860-522-0163	mcorcoran@gsofct.org or rkopylec@gsofct.org			
Phone Number	Email Address			
Property Owner(s) Name <i>(if not the applicant)</i>	Mailing Address			
Phone	Email Address			
Applicant's Interest in the Land (if other than own	ier)			
Is this property part of an approved subdivision?	✓ No Yes If YES , please state the name:			
2. Proposed Activity Information * The	ese questions are mandatory			
Check all activities occurring within 50 feet o	of wetlands or 100-feet of watercourses.			
Remove soil Deposit fill	Divert surface water			
Construction Grade	Construct a road or driveway			
Remove Vegetation 🖌 Restore Vegetat	ion Place a prefabricated structure			
Alter a watercourse Enhance a wate	rcourse Create a watercourse			
Remedy pollution Dredging or con	struct a dam Other			
* Describe the proposed activity. (use additional paper if necessary)				
Improvements are centered at the camp core and aim to improve accessibility, connectivity, and comfort for campers and staff. The main improvements include a renovated &				
expanded dining hall, new parking lot, new shower house, new cabins, paved access drive, and an accessible waterfront. Refer to narrative & site plans for detailed information.				

* What is the proposed use? (use additional paper if necessary)

The proposed use of the site will remain a Girl Scout camp facility with the majority of

activity occurring during the summer months for resident and day campers.

3. Wetland and Upland Review Area Information * These questions are mandatory

* What is the total area of the wetlands on the parcel? (see directions on page 7)	
38.5 acres (per online mapping tool)	

How often are the wetlands wet? All year Springtime only Sometimes I don't know A watercourse is defined as: Rivers, streams, brooks, waterways, lakes, ponds, marshes, swamps, bogs, and all other bodies of water, natural or artificial, vernal or intermittent, public or private. An upland review area is defined as: An area extending a minimum of 50-feet from the edge of wetlands and/or 100-feet from any watercourse (refer to regulations when doubling of an upland review area is required). st Square feet of disturbance in wetland, watercourse, or upland review area. (list areas separately) The upland review area of the wetland boundary associated with Sweetheart Lake has been depicted on all plans to the 200 foot limit due to the surrounding area having steep slopes. The regulated activity within the 200' upland review area is 1.12 acres/48,995 sf. Regulated activity within the 50 foot upland review area of Wetland 'X' as defined in the wetland delineation report is 0.09 acres/3,781 sf What is the square feet of any areas of enhancement within the upland review area? Removal of tent platforms within Wetland 'X' URA = 0.06 acres / 2,700 sf. Tree plantings and native seed mixes proposed within the URA are approximately 0.14 acres / 6,000 sf. An intermittent watercourse is defined as: A permanent channel and bank and the occurrence of two (2) or more of the following characteristics: scour, deposits of organic material, presence of standing water for a duration longer than a particular storm event, or hydrophytic vegetation. * Does the wetland have a watercourse through it? 🖌 No If YES, how often is the watercourse present? All year Springtime only Sometimes I don't know * Is there a pond, lake, or river on the property? (check all that apply) River Pond Lake None What is the total area of disturbance of an open water body? 0square feet 0 What is the **linear feet** of disturbance of a watercourse? feet Has the property been delineated by a Certified Soil Scientist? No 🖌 Yes

What is wetland delineation?

If YES, what year did the delineation occur? 2022

Delineation is an act of locating the boundary or border of a wetland or waterbody. Delineation also includes describing the functions and values the water system provides the geographical location. In the state of Connecticut only a certified Soil Scientist is recognized as being able to perform a wetland or watercourse delineation.

4. Alternatives

* Please explain to the Commission the reason you chose this location for your proposed activity or project. What alternatives have been considered to avoid altering wetlands or watercourses? (use additional paper if necessary)

* This question is mandatory

The project areas have been selected based primarily on the location of existing site features.

The majority of proposed renovations and upgrades are connected to existing camp buildings, access ways and activity areas.

The proposed work has been strategically located outside upland review areas where possible and with no direct wetland or watercourse impacts.

5. Abutters

Providing abutters only applies if the application requires a public hearing. Tolland's Planning & Development Department will supply the applicant with the names and addresses of adjacent property owners. There is a public hearing fee of \$300.

6. Site Plan Maps * Application Requirement

See page 7 below.

7. Additional Information

Supply any other information that would help in the understanding of the proposed activity.

8. A Complete Application Consists Of

- 1. This permit application fully filled out.
- 2. Site Plan Maps as described on page 7.
- 3. Signatures & Seals of licensed or certified professionals.
- 4. Filing fee
- 5. One (1) electronic copy of the application.
- 6. Nine (9) hard copies of the application.

Site Plan Maps * Application Requirement

Hand drawn or engineered plans?:

Depending on the proposed scope of work, hand drawn maps & plans may be acceptable **OR** professional survey/engineering drawings may be required. The IWWC or its duly authorized agent may waive any portion of these requirements.

Typical required site plan elements:

- A North Arrow
- A Legend

In the lower right hand corner showing the following information (Title Block):

- Name of Project and Address
- Name of Applicant/Owner/Developer
- Map Scale
- Name or initials of who prepared the plan (if not the applicant)
- Date prepared (or revision dates)

MAP 1: General Location Map (1 copy) – Refer to Page 7

- Use Tolland's GIS mapping system currently found on the Town's website, or on the Planning & Development webpage, click here.
- Turn on the themes and choose BOTH: "Wetlands Delineated" and "Wetlands Soils."
- Add Topography For online mapping choose BOTH "Topography" and "Topography 2016".
- Click on the property of interest
- Scale the map to 1"= 200 feet Refer to Page 7
- Print out the document or save electronically as a PDF

MAP 2: Existing Conditions (1 electronic / 9 hardcopies)

Scale: Up to 1'' = 100 feet (if conditions do not fit on a 24"x36" sheet scale can be reduced to 1''=200')

Use either Tolland's GIS mapping system or an existing A2 Survey from your building file. Ask us.

- Follow steps 1-4 from above For online mapping.
- **T**opography
- Existing property lines for entire property
- Locate all regulated areas on property: wetlands, watercourses, upland review areas 50' or 100'
- Locate the existing well & septic locations (properties with public utilities mark the general location)
- Locate significant exiting features or structures, buildings, roads, driveways, stonewalls, easements, ledges, stone outcrops, etc.
- □ Total acreage of the property
- Wetland delineation may be required if a delineation occurred prior to 1990. Call us.

Mapping: On-line GIS

MAP 3: Proposed Site Plan (1 electronic / 9 hardcopies)

- **Scale:** Any scale between 20 scale 50 scale is acceptable (e.g. 1"=20 ft., 30 ft., 40 ft., 50 ft.)
- All items from Map 2 above
- Limits of disturbance (the boundary line where the proposed activity will occur including layout areas)
- Property setbacks
- Distance (linear feet) of proposed activity from property setbacks
- Area (square footage) of proposed activity within a regulated area (wetland, upland review area) if any
- Proposed buildings, structures, septic systems, roads (including logging roads), etc.
- Distance (linear feet) from proposed activity to closest regulated area
- Label edges and general areas of existing and proposed vegetation (forest, field, lawn, clearings)
- Temporary storage piles (e.g. fill, topsoil, organic soil)
- Erosion and sedimentation measures, and/or other measures planned to protect wetlands, watercourses from harmful discharges during or after the proposed activity. * This question is mandatory
- □ Signature and Seal of Surveyor, Landscape Architect or Professional Engineer * This is mandatory
- □ If wetlands have been delineated by a certified Soil Scientist the Signature and Certification Number must be on the plans * This is mandatory

Additional Site Plan Requirements for Projects deemed a "Significant Activity"

- A Public Hearing Fee of \$300 may be required
- An Engineer or Expert review fee may be required lack of payment are grounds for denial without prejudice for an incomplete application. Call us.
- Hydraulic modifications to wetlands or watercoureses (if any)
- □ Soil Scientist report including the observations of existing ecological communities, soil types

Type of Permit	Type of Permit Fee Amount	
Residential Uses – Existing Lots \$80.00 plus \$60.00 State Fee		\$140.00
Map Amendment	\$300.00 plus \$60.00 State Fee	\$360.00
Modify Previous Approval	\$100.00 plus \$60.00 State Fee	\$160.00
Appeal Agent Issued Permit\$80.00 plus \$60.00 State Fee		\$140.00
Wetlands Buffer Zone Markers Fee \$1.00 each		TBD
Other uses \$200.00 plus \$60.00 State Fee		\$260.00

Additional Fees:

Agent Issued Permits (Activity in Upland Review Area):

Fee \$40.00 plus \$60.00 State Fee (Total \$100.00)

Plus Advertisement Costs: Applicants must advertise in Journal Inquirer at own cost.

Subdivision without new roads or storm drainage:

Fee \$200.00 for first 2 lots, **plus** \$50.00 for each additional lot with proposed activity in regulated area **plus** \$60.00 State Fee.

Subdivision with New Roads:

\$200.00 **plus** \$50.00 for each additional lot with proposed activity in regulated area **plus** \$200.00 for each 1,000 linear feet of road (or any part thereof) **plus** \$60.00 State Fee.

Commercial, Industrial, Multi-Family Residential (as defined by Zoning Regulations) Fees:

- Up to 23,000 square feet impervious surface: \$400
- 23,001 to 50,000 square feet: \$400 plus \$5 per 1,000 square feet in excess of 23,000 square feet
- Over 50,000 square feet: \$535 plus \$2 per \$1,000 square feet in excess of 50,000 square feet required.

plus State Fee: \$60

Public Hearing Fee: (When it is determined a Public Hearing is required) \$300.00 (in addition to above fees, if above fee is less than \$500.00) -

Filing fees may include additional costs incurred by the Town of Tolland, including, but not limited to, the expense of retaining experts to analyze, review and report on areas requiring a detailed technical review in order to assist the Commission in its deliberations. Said costs will be estimated by the Commission, based on preliminary estimates from such experts, and said estimate of costs times 150% will be paid over to the Commission prior to proceeding on the application. Upon completion of the technical review and a determination of the costs incurred, any excess will be refunded to the applicants. The applicant shall not be responsible for costs incurred in excess of 150% of the Commission's estimate.

Signature and Authorization

I, as the applicant, do hereby certify that I am familiar with all the information provided in the application and I am aware, that an incomplete application form, as well as a lack of payment of all associated permit fees, are grounds for denial without prejudice by either the Commission or their designated agents.

I am aware of the penalties for obtaining a permit through deception or through inaccurate or misleading information.

I, as the owner, do hereby authorize the members and designated agents of the Inland Wetlands Commission and professionals hired by the Commission for the purpose of reviewing this application to inspect the property from this date forward until the permitted activity is completed or the application is denied.

I, as the applicant, do understand that an engineer review fee may be required and a lack of payment are grounds for denial without prejudice by either the Commission or their designated agents.

I further understand that the Commission may request further information in connection with this application and that if the proposed activity involves a significant activity, an additional filing fee of \$300 be required for a public hearing.

Rocky Kopylec	Digitally signed by Rocky Kopylec Date: 2023,10.12 10:39:58 -04'00'	10/12/2023	
Sie	gnature of Applicant	Date	
Signatu	re of Owner (if different)	Date	

For Office	Use			
FEE TOTALS				
Amount:				
Paid:				
Agent Issued or Commission Issued:				
Date received by Land Use Department:				
Date received by Commission:				

Camp Yankee Trails Inland Wetlands Application Project Narrative

Camp Yankee Trails has sat idle and unused by GSofCT for several decades; however, with the sale of other camp properties the organization has decided to reinvest in Camp Yankee and relocate their only resident camp experience in Connecticut to the property. To do so, the property needs several upgrades to buildings, infrastructure, and the site.

The buildings to be upgraded or built new include renovations and additions to the dining hall, a new shower house, and four new cabins including an accessible unit. The building improvements are consolidated in the camp core and are centered around the existing dining hall. The dining hall will be renovated with a new kitchen, bathrooms, storage, and larger dining area. The building will be insulated and heated to accommodate year-round use. To further support the camp and dining hall area a new parking lot is proposed to accommodate 49 cars. GSofCT hopes that the property will not only be used as a resident camp but can also host staff events, girl scout meetings, and outside events year round. Currently the small dirt lot can accommodate, at most, a dozen vehicles.

The shower house and camp cabins will be seasonal structures constructed to the west and north of the dining hall and parking lot. Keeping each of these uses central to each other allows for ease of access, consolidates infrastructure needs, and reduces overall impacts to the site. Accessible stone dust and concrete paths will connect each of the improvement areas furthering the goal of a property for all users.

As with most summer camps a key feature is water play, so GSofCT is looking to improve the accessibility and usability of the existing waterfront on Sweetheart Lake. The current waterfront area is steep with uneven terrain and a small "beach" area that is prone to erosion. The proposed waterfront improvements will allow for ADA compliant access via a series of ramps and sloped walks which necessitate the construction of retaining walls. The retaining walls also allow for the grade of the waterfront area to be improved to increase the beach area and provide a consistent slope down to the water's edge.

Construction is anticipated to begin in the winter of 2023 with most improvements completed by June 2024. The anticipated sequence of construction is:

- 1. Install sediment and erosion controls.
- Clear and grub trees and vegetation to the indicated clearing limits. Wherever possible, trees will be preserved. Clear cutting areas is not the goal of the project; however, some areas require full removal to accommodate the improvements. Several areas also have hazardous trees that need to be removed for safety reasons.
- 3. Pad out access drive and parking area to allow for construction access and compaction of subbase materials.
- 4. Selective demolition of dining hall
- 5. Installation of underground utilities surrounding building footprints and within parking lot
- 6. Construction of shower house and dining hall additions
- 7. Extension of utilities to necessary end points including septic leaching fields and drainage structures
- 8. Construction of cabins
- 9. Fine grading and installation of walking paths
- 10. Install landscaping
- 11. Finalize construction of parking lot and access road
- 12. Construct waterfront improvements (with lake still drawn down)
- 13. Remove sediment and erosion controls and clean site

CAMP YANKEE TRAILS SITE IMPROVEMENTS

343 PLAINS ROAD TOLLAND, CONNECTICUT

REGULATORY DRAWINGS

NOVEMBER 21, 2023



Carl de

15

Le.

1.6.4

- 1. BOUNDARY INFORMATION IS BASED UPON FIELD SURVEY CONDUCTED BY: GARDNER & PETERSON ASSOCIATES, LLC TOLLAND, CONNECTICUT, TAKEN FROM A MAP ENTITLED PERIMETER SURVEY LAND OF THE GIRL SCOUTS OF CONNECTICUT, INC. 343 PLAINS ROAD, TOLLAND, CONNECTICUT, PREPARED FOR GIRL SCOUTS OF CONNECTICUT AT A SCALE OF 1"=100', DATED: 11-09-2022
- 2. TOPOGRAPHIC INFORMATION IS BASED ON AERIAL SURVEY CONDUCTED BY AERIAL SURVEYS INC. WATERBURY, CONNECTICUT 06708, PREPARED FOR GIRL SCOUTS OF CONNECTICUT ON APRIL 29, 2022.
- 3. INFORMATION REGARDING THE LOCATION OF EXISTING UTILITIES HAS BEEN BASED UPON AVAILABLE INFORMATION REGARDING THE LOCATION OF EXISTING UTILITIES HAS BEEN BASED UPON AVAILABLE INFORMATION AND MAY BE INCOMPLETE, AND WHERE SHOWN SHOULD BE CONSIDERED APPROXIMATE. THE LOCATION OF ALL EXISTING UTILITIES SHOULD BE CONFIRMED PRIOR TO BEGINNING CONSTRUCTION. CALL "CALL BEFORE YOU DIG", 1-800-922-4455. ALL UTILITY LOCATIONS THAT DO NOT MATCH THE VERTICAL OR HORIZONTAL CONTROL SHOWN ON THE PLANS SHALL IMMEDIATELY BE BROUGHT TO THE ATTENTION OF THE ENGINEER FOR RESOLUTION.
- 4. SLR CONSULTING US LLC. ACCEPTS NO RESPONSIBILITY FOR THE ACCURACY OF MAPS AND DATA WHICH HAVE BEEN SUPPLIED BY OTHERS.
- 5. INLAND WETLAND BOUNDARY WAS FLAGGED BY: MATTHEW SANFORD, REGISTERED SOIL SCIENTIST INLAND WETLAND BOUNDARY WAS FLAGGED BY: MATTHEW SANFORD, REGISTERED SOLL SCIENTIST AND PRODESSIONAL WETLAND SCIENTIST, AND MEAGHAN FOCARTY, ENVIRONMENTAL SCIENTIST, BOTH OF SLR INTERNATIONAL CORPORATION ON OCTOBER 07, 2022 AS SHOWN ON DRAWING PERIMETER SURVEY LAND OF THE GIRL SCOUTS OF CONNECTICUT, INC. 343 PLAINS ROAD, TOLLAND, CONNECTICUT, DATED 11-09-2022 AND FIELD LOCATED BY GARDNER & PETERSON ASSOCIATES, LLC, 178 HARTFORD TURNPIKE TOLLAND, CONNECTICUT ON NOVEMBER 1, 2022.
- 6. ALL UTILITY SERVICES ARE TO BE UNDERGROUND. THE EXACT LOCATION AND SIZE OF ELECTRIC, TELEPHONE, CABLE TELEVISION AND GAS ARE TO BE DETERMINED BY THE RESPECTIVE UTILITY COMPANIES.
- ALL DIMENSIONS AND ELEVATIONS SHALL BE VERIFIED IN THE FIELD PRIOR TO CONSTRUCTION, ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER
- SEDIMENT AND EROSION CONTROL MEASURES AS DEPICTED ON THESE PLANS AND DESCRIBED WITHIN THE SEDIMENT AND EROSION CONTROL NARRATIVE SHALL BE IMPLEMENTED AND MAINTAINED UNTIL PERMANENT COVER AND STABILIZATION IS ESTABLISHED. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL CONFORM TO THE "GUIDELINES FOR SOL EROSION AND SEDIMENT CONTROL, CONNECTICUT 2002, AND IN ALL CASES BEST MANAGEMENT PRACTICES SHALL PREVAIL.
- 9. ALL DISTURBED AREAS SHALL RECEIVE A MINIMUM OF 6" TOPSOIL, AND BE SEEDED WITH GRASS OR SODDED, AS SHOWN ON THE PLANS.
- 10. ALL STORM DRAIN PIPE SHALL BE SMOOTH LINED CORRUGATED PLASTIC PIPE (SLCPP) UNLESS OTHERWISE INDICATED.
- 11. ALL PROPOSED CONTOURS AND SPOT ELEVATIONS INDICATE FINISHED GRADE.
- 12. ALL GRAVITY SANITARY SEWER PIPE SHALL BE PVC SDR35 UNLESS OTHERWISE INDICATED. 13. ALL CONSTRUCTION MATERIALS AND METHODS SHALL CONFORM TO THE TOWN OF TOLLAND REQUIREMENTS AND TO THE APPLICABLE SECTIONS OF THE STATE OF CONFICUENT DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS FOR ROADS, BRIDGES, AND INCIDENTAL CONSTRUCTION, FORM 818 AND ADDENDUMS
- 14. ALL GUTTERS, ROOF DRAINS AND FOUNDATION DRAINS SHALL BE TIED INTO THE PROPOSED STORM DRAINAGE SYSTEM.
- 15. THE PLANS REQUIRE A CONTRACTOR'S WORKING KNOWLEDGE OF LOCAL, MUNICIPAL, WATER I THE PARTS REQUIRE A CONTRACTORS TO STATUS AND A CONFLICTS BETTAL MUTLER AND A CONFLICTS BETTALS AND AUTHORITY, AND STATE CODES FOR UTILITY SYSTEMS. ANY CONFLICTS BETTALE AN ATERIALS AND LOCATIONS SHOWN, AND LOCAL REQUIREMENTS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO THE EXECUTION OF WORK. THE ENGINEER WILL NOT BE HELD LIABLE FOR COSTS INCURRED TO IMPLEMENT OR CORRECT WORK WHICH DOES NOT CONFORM TO LOCAL CODE.
- 16. ALL FUEL, OIL, PAINT, OR OTHER HAZARDOUS MATERIALS SHOULD BE STORED IN A SECONDARY CONTAINER AND REMOVED TO A LOCKED INDOOR AREA WITH AN IMPERVIOUS FLOOR DURING NON-WORK HOURS.
- 17. COMPLIANCE WITH THE PERMIT CONDITIONS IS THE RESPONSIBILITY OF BOTH THE CONTRACTOR AND THE PERMITTEE.
- 18. PERIMETER SWALES AND RESPECTIVE SILTATION BASINS SHALL BE COMPLETED AND RESTORED PRIOR TO PROCEEDING WITH OTHER SITE CONSTRUCTION.ONST
- 19. THE PROPERTY OWNER MUST MAINTAIN (REPAIR/REPLACE WHEN NECESSARY) THE SILTATION CONTROL UNTIL ALL DEVELOPMENT ACTIVITY IS COMPLETED AND ALL DISTURBED AREAS ARE PERMANENTLY STABILIZED.



PROJECT SITE VICINITY MAP:









ZONING DATA TABLE ZONE: NATURAL RESOURCE PROTECTION AREA (WITHIN RDD)

USE: YOUTH CAMP

REQUIRED	EXISTING	PROPOSED
1,742,400 SF MIN. / 40 ACRES MIN.	11,135,840 SF / 255.64 ACRES	11,135,840 SF / 255.64 ACRES
200 FT. MIN.	<200 FT.	<200 FT.
100 FT. MIN.	<100 FT.	<100 FT.
15% MAX.	>15%	>15%
	REQUIRED 1,742,400 SF MIN. / 40 ACRES MIN. 200 FT. MIN. 100 FT. MIN. 15% MAX.	REQUIRED EXISTING 1,742,400 SF NIN., 11,135,840 SF,125.64 ACRES 40 ACRES MIN., 11,135,840 SF,125.64 ACRES 200 FT, MIN. 4200 FT. 100 FT, MIN. <200 FT.

PARKING DATA - DINING HALL

	EXISTING	PROPOSED
STANDARD SPACES	10	46
HANDICAP/ VAN ACCESSIBLE PARKING SPACES	1	3
TOTAL PARKING SPACES	11	49

PREPARED FOR:

GIRL SCOUTS OF CONNECTICUT, 340 WASHINGTON, STREET HARTFORD, CT 06106

LIST OF DRAWINGS

NO.	NAME	TITLE
00		TITLE SHEET
01	IN	INDEX PLAN
02-04	EX-1-3	EXISTING CONDITIONS
05	RA-1	REGULATED ACTIVITY
06	SP-1	SITE PLAN - OVERALL
07	SP-2	SITE PLAN - WATERFRONT
08	SP-3	SITE PLAN - DINING HALL & CAMP UNITS
09	SP-4	SITE PLAN - WATERFRONT ENLARGEMENT
10	LS-1	LANDSCAPING - WATERFRONT
11	LS-2	LANDSCAPING - DINING HALL & CAMP UNITS
12	GR-1	GRADING - OVERALL
13	GR-2	GRADING - WATERFRONT
14	GR-3	GRADING - DINING HALL & CAMP UNITS
15	GR-4	GRADING - WATERFRONT ENLARGEMENT
16-17	UT-1-2	SITE PLAN - UTILITIES
18-19	SE-1-2	SEDIMENT & EROSION CONTROLS
20	SE-3	SEDIMENT & EROSION CONTROL NOTES & DETAILS
21-25	SD-1-5	SITE DETAILS
26	PR-4	ROAD PROFILE
27	SV-1	BOUNDARY SURVEY



















PLANTING NOTES

.

.

- 1. THE CONTRACTOR SHALL VERIFY THE LOCATION OF ALL UNDERGROUND UTILITIES PRIOR TO EXCAVATING PLANT PITS.
- SEED ALL DISTURBED AREAS TO LAWN UNLESS OTHERWISE NOTED. THE CONTRACTOR SHALL PROVIDE A 6" MINIMUM DEPTH OF SCREENED TOPSOIL, AS SPECIFIED, FOR ALL LAWN AREAS. AS NOTED ON THE DETAILS, SUBGRADE BENEATH PROPOSED LAWN AREAS SHALL BE LOOSENED OR SCARIFIED TO A MINIMUM DEPTH OF 24 INCHES.
- 3. ALL PLANTING BEDS SHALL HAVE 12" MINIMUM DEPTH OF TOPSOIL.
- THE CONTRACTOR SHALL PROVIDE A 4" MIN. DEPTH OF SHREDDED BARK MULCH OVER ALL PLANTING BEDS AND TREE PLANTINGS. MULCHED PLANT BEDS SHALL EXTEND 12" FURTHER THAN THE ADJACENT PLANTINGS. NO DYED MULCH. 4.
- ALL PLANT MATERIAL IS SUBJECT TO INSPECTION AND APPROVAL BY THE LANDSCAPE ARCHITECT PRIOR TO AND AFTER PLANTING. 5.
- 6. PLANT SPECIES MAY BE ADJUSTED BASED ON AVAILABILITY AT TIME OF PLANTING. ALL PLANT MATERIAL SUBSTITUTIONS ARE SUBJECT TO REVIEW AND APPROVAL BY THE LANDSCAPE ARCHITECT.
- ALL PLANT MATERIALS SHALL CARRY A FULL GUARANTEE FOR A PERIOD OF ONE YEAR FROM THE DATE OF ACCEPTANCE, TO INCLUDE PROMPT TREATMENT OR REMOVAL AND REPLACEMENT OF ANY PLANTS FOUND TO BE IN AN UNHEALTHY CONDITION BY THE LANDSCAPE ARCHITECT. ALL REPLACEMENTS SHALL BE OF THE SAME KIND AND SIZE OF PLANTS SPECIFIED IN THE PLANT LIST.
- 8. MAINTENANCE SHALL BEGIN IMMEDIATELY AFTER PLANTING AND SHALL CONTINUE UNTIL ACCEPTANCE BY THE LANDSCAPE ARCHITECT AT THE END OF THE WARRANTY PERIOD. MAINTENANCE SHALL INCLUDE WATERING, MULCHING, TIGHTENING & REPLACING OF GUYS, REPLACEMENT OF SICK OR DEAD PLANTS, RESETTING PLANTS TO PROPER GRADE OR UPRIGHT (PLUMB) POSITION, RESTORATION OF SAUCERS, AND ALL OTHER CARE NEEDED FOR PROPER GROWTH OF THE PLANTS.
- 9. WHERE A SIZE RANGE IS SPECIFIED AT LEAST 50% OF PLANTS PROVIDED SHALL BE OF THE LARGER SIZE.
- 10. CONTRACTOR TO REMOVE TREE STAKES AFTER ONE GROWING SEASON.
- 11. TAKE NOTE TO PROTECT ROOT ZONES OF EXISTING TREES ROOT ZONES DURING CONSTRUCTION AS SHOWN ON PLANS.





				J.S.		
And a second	7. 19					SLR Surry Cont Control Cont Control Cont Control Cont Control Cont Control Cont Control Cont Control Cont Control Control Control Control Control Control Control Control Cont
A COLOR		AB AB				DESCRIPTION DATE BY
		SEED TO LAWN				
PLANT SCHE		LE WATERFRONT	COMMON NAME WHITE SPRUCE	<u>SIZE</u> 6' HT. MIN.	CONT. B&B	TERFRONT
'S <u>)RNAMENTAL TREES</u> CC	1 <u>QTY</u> 2	PINUS STROBUS BOTANICAL NAME CERCIS CANADENSIS CERCIS CANADENSIS CERCIS CANADENSIS	WHITE PINE <u>COMMON NAME</u> EASTERN REDBUD BUIDGUNDY HEADTE EASTERN REDBUD	6' HT. MIN. SIZE 8'/10' HT. 8'/10' HT.	B&B <u>CONT.</u> B&B B&B	G - WA TRAILS MENTS CTICUT
T D <u>HADE TREES</u> AB AL AC DP	1 1 <u>QTY</u> 3 1 2 2	CERCIS CARADENSIS 'BURGUNDY HEARTS' CORNUS FLORIDA 'CHEROKEE CHIEF' BOTANICAL NAME ACER RACRUBRUM 'BRANDYWINE' ACER SACCHARUM 'LEGACY' AESCULUS X CARNEA 'BRIOTII' OLIFECIS PAULISTPIS	COMMON NAME BRANDYVINE RED MAPLE LEGACY SUGAR MAPLE BRIDGAR MAPLE BRIDTII RED HORSECHESTNUT PIN OAK	8 /10 HT. 8 /10 HT. <u>SIZE</u> 2.5"-3.0" CAL. 2.5"-3.0" CAL. 2.5"-3.0" CAL.	585 888 888 888 888 888 888	NDSCAPIN(MP YANKEE E IMPROVEN PLAINS ROAD LAND, CONNE
KL	<u>QTY</u> 15	BOTANICAL NAME KALMIA LATIFOLIA	COMMON NAME MOUNTAIN LAUREL	SIZE CONT.	<u>CONT.</u> #3	
Y <u>ERENNIALS</u> AI AN DP EG	<u>QTY</u> 17 11 21 20	BOTANICAL NAME ASCLEPIAS INCARNATA ASTER NOVAE-ANGLAE DENNSTAEDTIA PUNCTILOBULA EUTHAMIA GRAMINIFOLIA	COMMON NAME SWAMP MILKWEED NEW ENGLAND ASTER HAYSCENTED FERN GRASS-LEAFED GOLDENROD	SIZE CONT. CONT. CONT. CONT.	CONT. #1 #1 #1 #1 #1	MTD PJP MTD сезонер сачим о-со-ер 1"=30' сачим сачим scчие NOVEMBER 21, 2023 2023
NEW EN PRODUC	GLAND I ED BY N L LANE HADLEY	ROSION CONTROL/RESTORATION MIX 4,16 IEW ENGLAND WETLAND PLANTS MA 01075	i1 SF			але 141.13280.00006 рядаетно
(413)-54 ALL DISTURBED AR 3Y ERNST CONSERV	I8-8000 EAS DI /ATION	ESIGNATED AS LAWN SHALL BE SEEDE I SEEDS	D WITH 5311 CONSERVATION MIX			10 OF 26



















PERMANENT VEGETATIVE COVER

IN GENERAL, ALL CONSTRUCTION ACTIVITIES SMALL PROCEED IN SUCH A HAINER SO AS NOT TO POLLUTE AVY WETANDS, WATERCOURSE, WATERCOUX, AND CONDUT CAREYING WATER, ETC. THE CONTRACTOR SMALLINT, INSORAR AS POSSIBLE, THE SURFACE AREA OF EARTH MATERIALS PROSED BY CONSTRUCTION HETHODS AND IMMEDIATELY PROVIDE PERMANENT AND TEMPORARY POLLUTION CONTROL MEASURES TO

PERMANENT VEGETATIVE COVER SHALL BE ESTABUSIED AS VARIOUS SECTIONS OF THE PROJECT ARE COMPLETED IN ORDER TO STABULZE THE SOLL, REDUCE DOWNSTREAM DANAGE FROM SEDIMETE AND RUNOFF, AND TO INIANCE THE ASSIMETIC ATMERE OF THE SITE. IT MULL BE ARAULED TO ALL CONSTRUCTION AREAS SUDICT TO FROSION WHERE FIRML GRADING MAS BEEN COMPLETED AND A FEMAMERIC COVER IS NEEDED. SITE PREPARATION

2. INSTALL REQUIRED SURFACE WATER CONTROL MEASURES.

- 3. REMOVE LOOSE ROCK, STONE, AND CONSTRUCTION DEBRIS FROM AREA
- 4. PERFORM ALL PLANTING OPERATIONS PARALLEL TO THE CONTOURS OF THE SLOPE
- 5. AFFLY TOPSOIL AS INDICATED ELSEWHERE HEREIN
- 6. AFFLY FERTILIZER ACCORDING TO SOIL TEST OR:
- SPREAD SEEDING: WORK DEEPLY IN SOIL, BEFORE SEEDING, 300 LBS. OF 10-10-10 FERTULIZER PER ACRE (7 LBS. PER 1,000 SQ. FT.); THEW SIX (6) TO EIGHT (8) WEEKS LATER, AFELY ON THE SURFACE AN ADDITIONAL 300 LBS. OF 10-10-10 FERTILIZER PER ACRE. AFTER SEPTEMBER 1, TEMPORARY VEGETATIVE COVER SHALL BE AFFLED.
- FALL SFEDING: WORK DEEPLY IN SOIL, BEFORE SEEDING, 600 LBS. OF 10-10-10 FERTUIZER PER ACRE (14 LBS. PER 1,000 SQ. FT.).
- **VEGETATIVE COVER SELECTION & MULCHING**

TENPORARY VEGETATIVE COVER

PERENNIAL RYEGRASS 3 LBS./1,000 SQ.FT. (IOLUIUM PERENNE)

PERHANENT VEGETATIVE COVER:

AS SPECIFIED

TEMPORARY MULCHING

STRAY OR HAY 70-90 LBS./1,000 SQ.FT. (TEMPORARY VEGETATIVE AREAS)

WOOD FIBER IN HYDRONULCH SLURRY 25-50 LBS /1,060 SQ. FT.

- SMOOTH AND FIRM SEEDED WITH CULTIPACKER OR OTHER SIMILAR EQUIPMENT FRIOR TO SEEDING (EXCEPT WHEN HYDROSEEDING).
- SELECT ADAPTED SEED MIXTURE FOR THE SPECIFIC SITUATION. NOTE RATES AND THE SEEDING DATES (SEE VEGETATIVE COVER SELECTION & MULCHING SPEC, BELOW).
- AFFLY SEED UNIFORMLY ACCORDING TO RATE INDICATED, BY BROADCASTING, DRILLING, OR HYDRAULIC AFFLICATION.
- COVER GRASS AND LEGUME SEED WITH NOT MORE THAN 1/4 IIKCH OF SOIL. WITH SUITABLE EQUIPMENT (EXCEPT WHEN HYDROSEEDING).
- MULCH IMREDIATELY AFTER SEEDING, IF REQUIRED, ACCORDING TO TEMPORARY MULCHING SPECIFICATIONS. (SEE VEGETATIVE COVER SELECTION & MULCHING SPECIFICATION BELOW).
- 6. USE PROPER INOCULANT ON ALL LEGUNE SEEDINGS, USE FOUR (4) TIMES NORMAL RATES WHEN
- USE SOD WHERE THERE IS A HEAVY CONCENTRATION OF WATER AND IN CRITICAL AREAS WHERE IT IS IMPORTANT TO GET A QUICK VEGETATIVE COVER TO PREVENT EROSION.
- MAINTENANCE
- 1. TEST FOR SOIL ACIDITY EVERY THREE (3) YEARS AND LIKE AS REQUIRED
- ON STTES WHERE GRASSES FREDOMINATE, BROADCAST ANNUALLY 500 POUNDS OF 10-10-10 FERTULZER PER ACRE (12 LBS, FER 1,000 SQ. FT.) OR AS NEEDED ACCORDING TO ANNUAL SOIL TESTS.
- ON SITES WHERE LEGUMES PREDOMINATE, BROADCAST EVERY THREE (3) YEARS OR AS INDICATED BY SOIL TEST 300 POUNDS OF 0-20-20 OR EQUIVALENT PER ACRE (8 LBS PER 1,000 SQ. FT.). EROSION CHECKS

GENERAL

HYDROSEEDING

TEM-DRARY FERVIOUS BARRIERS USING BALES OF HAY OR STRAW, HELD IN PLACE WITH STAKES DRIVEN THROUGH THE BALES AND INTO THE GROUND OR GEOTEXTILE FARRIE FASTENED TO A FEACE POST AND BURIED INTO THE GROUND, SHALL BE INSTALLED AND MAINTAINED AS REQUIRED TO CHECK EROSION AND REDUCE SECURENTATION.

CONSTRUCTION

- 1. BALES SHOULD BE PLACED IN A ROW WITH ENDS TIGHTLY ABUTTING THE ADJACENT BALES.
- 2. EACH BALE SHALL BE EMBEDDED THTO THE SOIL A MINIMUM OF FOUR (4*) INCHES
- 3. BALES SHALL BE SECURELY ANCHORED IN FLACE BY WOOD STAKES OR. REINFORCEMENT BARS DRIVEN THROUGH THE BALES AND INTO THE GROUND. THE FLAST STAKE IN EACH BALE SHALL BE ANGLED TOWARD THE FLAXINGSLY LIND BALL TO FORCE BALES TOGETHER.
- GEOTEXTILE FABRIC SHALL BE SECURELY ANCHORED AT THE TOP OF A THREE FOOT (3') HIGH FENCE AND BURLED A MHINGH OF FOUR INCHES (4') TO THE SOLL SEAHS BETWEEN SECTIONS OF FILTER FABRIC SHALL OFFELMEN A MUNIMUN OF TWO FEET (2).
- INSTALLATION AND MAINTENANCE:
- 1. BALED HAY EROSION BARRIERS SHALL BE INSTALLED AT ALL STORM SEWER INLETS
- BALEO HAY EROSION BARRIERS AND GEOTEXTILE FERCE SHALL BE INSTALLED AT THE LOCATION INDICATED ON THE PLAN AND IN ADDITIONAL AREAS AS MAY BE DEEMED APPROPRIATE DURING CONSTRUCTION.
- 3. ALL EROSION CHECKS SHALL BE MAINTAINED UNTIL ADJACENT AREAS ARE STABILIZED
- INSPECTION SHALL BE FREQUENT (AT MINIMUM MONTHLY AND BEFORE AND AFTER REAVY RAIN) AND REPAIR OR REPLACEMENT SHALL BE MADE FROMPTLY AS NEEDED.
- 5. EROSION CHECKS SHALL BE REMOVED WHEN THEY HAVE SERVED THEIR USEFULNESS 50 AS NOT TO BLOCK OR DIPEDE STORIAWATER FLOW OR DRAINAGE.



	······			
EROSION CONTROL MEASURE	CONTROL OBJECTIVE	INSPECTION/MAINTENANCE	FAILURE INDICATORS	REMOVAL
SILT FENCE (SF) (RELATED: IP, STK)	- INTERCEPT, AND REDIRECT/DETAIN SMALL AMOUNTS OF SEDIMENT FROM SMALL DISTURBED AREAS. - DECREASE VELOCITY OF SHEET FLOW. - PROTECT SENSITIVE SLOPES OR SOILS FROM EXCESSIVE WATER FLOW.	INSPECT AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL OF 0.5 INCHES OR MORE. ACCUMULATED SEDIMENT MUST BE REMOVED ONCE ITS DEPTH IS EQUAL TO % THE TRENCH HEIGHT. INSPECT FREQUENTLY DURING PUMPING OPERATIONS IF USED FOR DEWATERING OPERATIONS.	PHYSICAL DAMAGE OR DECOMPOSITION EVIDENCE OF OVERTOPPED OR UNDERCUT FENCE EVIDENCE OF SIGNIFICANT FLOWS EVADING CAPTURE REPETITIVE FAILURE	SILT FENCE MAY BE REMOVED AFTER UPHILL AND SENSITIVE AREAS HAVE BEEN PERMANENTLY STABILIZED.
HAY BALES (HB)	- INTERCEPT, AND REDIRECT/DETAIN SMALL AMOUNTS OF SEDIMENT FROM SMALL DISTURBED AREAS. - DECREASE VELOCITY OF SHEEF FLOW. - PROTECT SENSITIVE SLOPES OR SOILS FROM EXCESSIVE WATER FLOW.	INSPECT AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL OF 0.5 INCHES OR MORE. ACCUMULATED SEDIMENT MUST BE REMOVED ONCE THE DEPTH OF SEDIMENT IS EQUAL TO W THE HEIGHT OF THE BARRIER. INSPECT FREQUENTLY DURING PUMPING OPERATIONS IF USED FOR DEWATERING OPERATIONS.	PHYSICAL DAMAGE OR DECOMPOSITION EVIDENCE OF OVERTOPPED OR UNDERCUT FENCE EVIDENCE OF SIGNIFICANT FLOWS EVADING CAPTURE REPETITIVE FAILURE	HAY BALES MAY BE REMOVED AFTER UPHILL AREAS HAVE BEEN PERMANENTLY STABILIZED,
CATCH BASIN INLET PROTECTION (IP)	- PROHIBIT SILT IN CONSTRUCTION-RELATED RUNOFF FROM ENTERING STORH DRAINAGE SYSTEM.	INSPECT AFTER ANY RAIN EVENT. IF FILTER BAG INSIDE CATCH BASIN CONTAINS MORE THAN 6" OF SEDIMENT, REMOVE SEDIMENT FROM BAG. CHECK SURROUNDING SILT FENCE AND HAY BALES PER NOTED ABOVE.	- RIPPED BAG - FAILED HAY BALES / SILT FERCE - SIGNIFICAIT SILT PRESENCE IN STORM DRAINAGE SYSTEM OUTFLOW.	INLET PROTECTION MAY BE REMOVED ONCE THE SITE HAS BEEN PERMANENTLY STABILIZED, AND ALL SECTIONS OF ROADWAY HAVE BEEN PERMANENTLY PAVED,
STOCKPILE PROTECTION (STK)	- RETAIN SOIL STOCKPILE IN LOCATIONS SPECIFIED, AND REDUCE WATER-TRANSPORT.	INSPECT SILT FENCE AT THE END OF EACH WORK DAY AND IMMEDIATELY REPAIR DAMAGES. PERIODIC REINFORCEMENT OF SILT FENCE, OR ADDITION OF HAY BALES MAY BE NECESSARY.	- EVIDENCE OF STOCK PILE DIMINISHING DUE TO RAIN EVENTS - FAILURE OF SILT FENCE	STOCKPILE PROTECTION MAY BE REMOVED ONCE THE STOCKPILE IS USED OR REMOVED.



FENCE POST (TYPICAL)

5.7-8



STABILIZE ENTIRE PILE WITH VEGETATION OR C SLOPE OR LESS

MIN, SLOPE MIN, SLOFE STRAWRALES OR SUITERICE

INSTAILATION NOTES

1. AREA CHOSEN FOR STOCKPILING OPERATIONS SHALL BE DRY AND STABLE. 2. MAXIMUM SLOPE OF STOCKPILE SHALL BE 1:2.

3. UPON COMPLETION OF SOLL STOCKPILING, EACH PILE SHALL BE SURROUNDED WITH EITHER SILF FENCING OR STRAWBALES, THEN STABILIZED WITH VEGETATION OR COVERED.

STOCKPILE PROTECTION (STK)

NOT TO SCALE

THE CONSTRUCTION OF THE PROJECT.

LAND GRADING

TOPSOILING

MATERIAL

APPLICATION

SITE PREPARATION:

ESTABLISHMEN

GENERA

SEDIMENT & EROSION CONTROL SPECIFICATIONS

PREVENT CONTAMINATION OF ADJACENT WETLANDS, WATERCOURSES, AND WATER BODIES, AND TO PREVENT, INSOFAR AS FOSSIBLE, EROSION ON THE SITE.

1. THE RESHAPING OF THE GROUND SURFACE BY EXCAVATION AND FILLING OR A COMBINATION OF BOTH, TO OBTAIN PLANNED GRADES, SHALL PROCEED IN ACCORDANCE WITH THE FOLLOWING CRITERIA:

THE CUT FACE OF EARTH EXCAVATION SHALL NOT BE STEEPER THAN TWO HORIZONTAL TO ONE VERTICAL (2:1).

c. THE CUT FACE OF ROCK EXCAVATION SHALL NOT BE STEEPER THAM ONE HORIZONTAL TO FOUR VERTICAL (1:4).

b. THE PERMANENT EXPOSED FACES OF FILLS SHALL NOT BE STEEPER THAN TWO HORIZONTAL TO ONE VERTICAL (2:1).

4. FROVISION SHOULD BE HADE TO CONDUCT SURFACE WATER SAFELY TO STORN DRAINS TO PREVENT SURFACE RUNOFF FROM DANAGING CUT FACES AND FILL SLOPES

e. EXCAVATIONS SHOULD NOT BE HADE SO CLOSE TO PROPERTY LINES AS TO ENDANGER ADJOINING PROPERTY WITHOUT PROTECTING SUCH PROPERTY FROM EROSION, SLIDING, SETTLING, OR CRACKING. f. NO FILL SHOULD BE FLACED WHERE IT WILL SLIDE OR WASH UPON THE PREMISES OF ANOTHER OWNER OR UPON ADJACENT WETLANDS, WATERCOURSES, OR WATER BODJES.

9. PRIOR TO ANY RE-GRADING, A STABILIZED CONSTRUCTION ENTRANCE SHALL BE PLACED AT THE ENTRANCE TO THE WORK AREA IN ORDER TO REDUCE MJD AND OTHER SEDIMENTS FROM LEAVING THE SITE.

TOPSOL SHALL BE SPREAD OVER ALL EXPOSED AREAS IN ORDER TO PROVIDE A SOIL MEDIUM HAVING FAVORABLE CHARACTERISTICS FOR THE ESTABLISHMENT, GROWTH, AND MAINTENANCE OF VEGETATION

1. TOFSOIL SHOULD HAVE FHYSICAL, CHEMICAL, AND BIOLOGICAL CHARACTERISTICS FAVORABLE TO THE GROWTH OF MANTS.

TOPSOIL SHOULD BE RELATIVELY FREE OF SUBSOIL MATERIAL AND MUST BE FREE OF STONES (OVER 1 DIAUETER), LUKES OF SOIL, ROOTS, TAEE LIMBS, TRASH, OR CONSTRUCTION DEBRIS. IT SHOULD BE EREE OF ROOTS OR RUISCUSES SUCH AS THISTIE, NUTRALS, MAD QUAXGRASS.

AN ORGANIC MATTER CONTENT OF SIX PERCENT (6%) IS REQUIRED. AVOID LIGHT COLORED SUBSOIL MATERIAL

SOLUBLE SALT CONTENT OF OVER 500 PARTS FER MILLION (PPM) IS LESS SUITABLE. AVOID TIDAL MARSH SOILS BECAUSE OF HIGH SALT CONTENT AND SULFUR ACIDITY.

6. THE pH SHOULD BE MORE THAN 6.0. IF LESS, ADD LIME TO INCREASE pH TO AN ACCEPTABLE LEVEL

SPREAD TOPSOIL UNIFORMLY TO A DEPTH OF AT LEAST SIX INCHES (6'), OR TO THE DEPTH SHOWN ON THE PLANS, DEFAILS AND SPECIFICATIONS.

TEMPORARY VEGETATIVE COVER SHALL BE ESTABLISHED ON ALL URFROTECTED AREAS THAT FRODUCE SEDJINHT, ACRAS WHERE FINAL GADDING HAS BEEN COMPLETED, AND AREAS WHERE THE ESTIMATED PERIOD OF BARE SOL EXPOSURE IS LISS STATU 12 MONTHS. PERIOD RE MER SOL EXPOSURE IS LISS STATU 12 MONTHS. PERIOD RE MER SOL EXPOSURE IS LISS STATU 12 MONTHS.

APPLY FERTILIZER ACCORDING TO SOIL TEST OR AT THE RATE OF 300 LBS. OF 10-10-10 FER ACRE (7 LB PER 1,000 SQ. FT.) AND SECOND APPLICATION OF 300 LBS. OF 10-10-10. (5 LBS. PER 1,000 SQ. FT.) WHEN GRASS 15 FOUR INCRES (4') TO STI MICHES (6') INGN. AFRY ONLY WHEN GRASS 15 FOR.

UNLESS HYDROSEEDED, WORK IN LINE AND FERTILIZER TO A DEPTH OF FOUR (4*) INCHES USING A DISK OR ANY SUITABLE EQUIFMENT.

SELECT APPROFRIATE SPECIES FOR THE SITURATION. NOTE RATES AND SHEDING DATES (SEE VEGETATIVE COVER SELECTION & NULCHING SPECIFICATION BELOW). 2. APPLY SEED UNIFORMUT ACCORDING TO THE PATE INDICATED BY READACASTING, DRILLING, OR HTDRAULD APPLICATION. 3. UNLESS INTROSEETED, COVER INTEGRASS SEEDS WITH NOT NORE THAN 1.4 INCH OF SOIL USING SUITABLE EQUIPMENT. 4. MULCH IMMEDIATELY AFTER SEEDING IF REQUIRED. (SEE VEGETATIVE COVER SELECTION & NULCHING SPECIFICATION BELOW). 3. APPLY STRAW OR HAY NULCH AND ANCIMOR TO SLOFES GREATER THAN 3% OR WHERE CONCENTRATED ATOM WILL OCCUR.

TILLAGE SHOULD ACHIEVE A REASOURDLY UNFORM LOOSE SEEDBED. WORK ON COUTOUR IF SITE IS SLOPING.

2. UPON ATTAINING FINAL SUBGRADES, SCARIFY SURFACE TO PROVIDE A GOOD BOND WITH TOPSOIL

3. REMOVE ALL LARGE STONES, TREE LIMBS, ROOTS AND CONSTRUCTION DEBRIS.

APPLY LIME ACCORDING TO SOIL TEST RECOMMENDATIONS

2. TOPSOTL SHOULD HAVE A SANDY OR LOAMY TEXTURE.

AVOID SFREADING WHEN TOPSOIL IS WET OR FROZEN

1. INSTALL REQUIRED SURFACE WATER CONTROL MEASURES

2. REMOVE LOOSE ROCK, STONE, AND CONSTRUCTION DEBRIS FROM AREA.

3. AFRLY DOLOMITIC LINESTONE ACCORDING TO SOIL TEST RECOMMENDATIONS

TEMPORARY VEGETATIVE COVER

GENERAL









.



SC-740 STORMTECH CHAMBER SPECIFICATIONS

- ERS SHALL BE STORMTECH SC-74
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-VODIFIED POLYFROPYLENE COPOLYMERS.
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMEER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREVENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE ASHTO LIFD BRDGE DESIGN SPECIFICATIONS, SECTION 1121, ZHE BHT FOR 11 (LOAD GUIRATION FLAD LOADS AND 3) SHORT-DURATION LIVE (LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IN AND JULTERE VEHICLE FREESENCES.
- CHAMEERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTIM F7787, "STADNARD PRACTICE FOR STRUCTURAL DES ON OF THERMOPLASTIC CORRUNATE WILL STORMINHER COLLECTION CHAMBERS", LOAD CONFIDURATIONS SHALL INCLUE: 11 INSTRUTANEOUS (~1 MAY ASHTO DESIGN TRUCK LINE LOAD CHAMINAU CONFR J) WAXMAN RETAVATENT (FXPR) COVER LOAD MOA 3) JLLOWABLE COVER WITH PRAVED (I-WEEK) ASHTO DESIGN T

CONCRETE COLLA

4

- JURE EVENTS FOR HANGING AND INSTALLATION: TO MAINTAN THE WORTH OF CHANNERED DRIKING SHIPPING AND HANDLING, CHANBERS SHALL HAVE IF DECOUL, HITERCOGNISTICATION DATA DATA THE AND AND BACKFELL, THE HEIGHT OF THE CHANBER HOLD THE WORTH OF CHANNER DRIKING AND BACKFELL, THE HEIGHT OF THE CHANBER JOHT SHALL NOT DE LESS THAN WAY. TO ENSURE THE WITERGRITY OF THE ARCH SHAPE DURING INSTALLATION, A) THE ARCH ST FFRESS CONSTANT AS DEFINED IN SECTION 28 20 A STATUSATION BASTALLATION, AND E GOULT DI SO LISSING, AND TO RESIST CHANGEN DEFORMATION DURING INSTALLATION AT ELEVATED THE PRIMINERG SUSCE TO FT THE CACHE DRIVEN DIALLATION AND REACHEST THAN ON BE GOULT DI SO LISSING, AND ITO RESIST CHANGEN DEFORMATION DURING INSTALLATION AT ELEVATED THE PRIMINERG SUSCE TO FT THE CACHEST DEFORMATION DURING INSTALLATION AT ELEVATED OR YELLOW COLOR
- ONLY CHANGERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER, THE CHANGER UNVERTITIER SHALL SUBJIT A STRUCTURE LEVILUATION FOR APPROVAL BEFORE DELYMING CHANGERS TO THE PROVINCET SITE AS
- LOWS: THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER. THE STRUCTURAL EVALUATION SHALL DE VUONSTRATE THAT THE SAVETY FACTORS ARE GREATER THAN OR EQUIL TO 15 STOR DE PADL IOAD AND 15 FOR LIVE LOAD. THE UNATUM REGURED BY ASTMET277 AND BY SECTORS 3 AND 212 OF THE ASSING URFD BROGE DESIGN SPECFEXITIONS FOR THERVORASTIC PIPE. THE TEST DERIVED ORGEP MODULUS AS SPECIFIED IN ASTMETARIA BALL BE USED FOR PERMANENT DEAD LOAD DEGISION DECENT THAT TAVALL BE THE TA-TAR MODULUS USED FOR DEDISON.
- 9. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

NNECTED THROUGH ANY CH

4" PVC INSPECTION PORT DETAIL

(SC SERIES CHAMBER)

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-740 SYSTEM

- STORMTECH SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLER:
- STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORWTECH SC-310 SC-740 DC-780 CONSTRUCTION GUIDE"
- CHAVBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUA CHAVBERS. STORVITECH RECONVENDS 3 BACKFILL METHODS. CHAVERS STORVITCE NERCONVENDS 3 BACKFLL VETHODS • STONESHOOTER LOCATED OFF THE CHAVERE BED • BACKFLL AS 60VS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE • BACKFLL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- MAINTAIN MINIMUM 6" (150 mm) SPACING BETWEEN THE CHAMBER ROWS
- EMBEDIVENT STONE SURROUNDING CHAVBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2* (20-50 mm).
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOVIVENDS THE USE OF "FLEXISTORIN CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORWATER MANAGEVENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORVTECH SC-310/SC-740/DC-760 CONSTRUCTION GUIDE".
- THE USE OF CONSTRUCTION EQUIPMENT OVER \$C740 CHAMBERS IS LIWITED: NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS NO RUBBER THEED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FALL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORWITEM SCALOSEO X00C-760
- WEIGHT UNITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- FULL 36" (300 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMUTECH STANDARD WARRANTY.

CONTACT STORVTECH AT 1-688-692-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

INSPECTION & MAINTENANCE

STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- ECT ISOLATOR ROW FULS FOR SEDMENT SPECTON FOR SEP FOR SEDMENT REMOVE AD CLAVIELES THAINE DRAIN LOWER A CAMERA INTO BOLATOR ROWIN LUS FOR VISIUL INSPECTION OF SEDMENT LEVELS (OPTIONLS) IN SEQUENT BAT, OR ABOVE, 200 mm) PROCEED TO STEP 2. F NOT, PROCEED TO STEP 3. LLISOLATOR FLUS ROWS. ULS ROLATOR FLUS ROWS. USANG A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATOR ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATOR ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATION ISOLATOR ROW FLUS IN TRONG THE ISOLATION OF ISOLATION ISOLATOR ROW FLUS IN TRONG TO ROW ISOLATION ISOLATION ISOLATOR ROW FLUS IN TRONG TO ROW ISOLATION ISOLATION ISOLATOR ROW ISOLATOR ROW ISOLATOR ROW ISOLATOR ROW IS
- B.1. B.2
- B.3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 A A FOED CULVERT CLEANING NOZZE WITH REAR FACING SPREAD OF 45° (1.1 m) OR WORE IS PREFERRED
 B. APPLY MULTIRE PASSES OF JETVICUTITE BACKFILUSH WATER IS CLEAN
 C. VACUUM STRUCTURE SUMP AS REQUIRED

STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.

STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM

NOTES

INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.

RUCTURAL ANGLE 3" x 2" x 1/2" IBED IN CONCRETE BLOCK AROUND RIMETER OF GRATING AND IVANIZED

1/2" DIA. x 3-1/8" H4L HEADED STUD @ 12" O.C.

2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT VAIN



RETE COLLAR NOT REQUIRED

EAG4(PKIT) O

8" NYLOPLAST INSPECTION POR

BODY (PART# 27) TRAFFIC RATED LOCKING COVER

4" (100 mm) SDR 35 PIPE

4" (100 mm) INSERTA TE TO BE CENTERED ON INSERTATE



AAS CL	DESCRIPTION	MATERIAL LOCATION		
	ANY SOLROCK MATERIALS, NATIVE SOLS, OR PER ENGINEER'S PLANS CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREVENTS.	FINAL FILL: FILL MATERIAL FOR LAYER D'STARTS FROM THE TOP OF THE 'C'LAYER TO THE BOTTOM OF FLEXIBLE PAXEMENT OR UNPAYED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE D'LAYER.	D	
3, 357, 4, 457, 5	GRANULAR WELL-GRADED SOLU/AGREGATE MXTURES, «33% FINES OR FROCESSED AGGREGATE. MOST PANEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	NITIAL FILL: FAL MATERIAL FOR LAYER (C' STARTS FROM THE TOP OF THE EVECUMENT STONE (B' LAYER) TO 16' (450 mm) ABOVE THE TOP OF THE CHANGER NOTE THAT PAREMENT SUBBASE MAY BE A PART OF THE C' LAYER	c	
3	CLEAN, CRUSHED, ANGULAR STONE	EMBEDMENT STORE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE (A' LAYER) TO THE 'C' LAYER ABOVE.	в	
3	CLEAN, CRUSHED, ANGULAR STONE	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	۸	



NOTES:

1

- PERIVETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.

- COLORS.







DETENTION BASIN OUTLET CONTROL STRUCTURE










.

NOT	ES:
NOT	ES:



NOTES:

- 1. THIS MAP AND SURVEY HAVE BEEN PREPARED IN ACCORDANCE WITH THE REGULATIONS OF CONNECTICUT STATE AGENCIES, SECTIONS 20-3006-1 THROUGH 20-3006-20. THIS IS A PERWIETE SURVEY BUSICE ON A DEPENDENT RESURVEY CONFORMING TO HORIZONTIAL ACCURACY CLASS A-2 EXCEPT FOR THE PROPERTY BOUNDARY BETWEEN THE SUBJECT PARCEL AND THE CERTIFICATION THE PROPERTY BOUNDARY BETWEEN THE SUBJECT CLASS COUP OF THE LACK VERYOUT RUNNARY INC. IS CERTIFICE TO HORIZONTIAL ACCURACY CLASS A-2 EXCEPT FOR THE PROPERTY BOUNDARY BETWEEN THE SUBJECT CLASS COUP OF THE LACK VERYOUT RUNNARY INC. IS CERTIFICE TO HORIZONTIAL ACCURACY CLASS COUP OF FUNCTION OF THE THE RUNNARY WAYS AND THE LACK OF FUNCTIAL BOUNDS LARKING THE RIGHT A WAY OF THE RUNNARY INC. SUBJECT OF FUNCTIAL BOUNDS LARKING THE RIGHT A WAY OF THE RUNNARY INC. SUBJECT OF FUNCTION. BOUNDS LARKING THE RIGHT A WAY OF THE RUNNARY INC. SUBJECT OF FUNCTION. BOUNDS LARKING THE RIGHT A WAY OF THE RUNNARY INC. SUBJECT INC. SUBJECT OF FUNCTION. BOUNDS LARKING THE RIGHT A WAY OF THE RUNNARY INC. SUBJECT INC. SUBJECT

- WAP REFERENCE:
 WARKING THE REGNA SECONT COUNCIL, INC. TOLLAND AND ELLINGTON, CONN⁴ BY WORTON S. FINE CML EXQUERE & LWD SURVEYOR, DATE 7 JUNE 1952. SCALE 1⁴-200⁵.
 B. "PLAN OF LAND PREPARED FOR STEPHEN D. WILLMANS IN TOLLAND, CONNECTICUT" BY CARDIER & FETESSON ASSOCIATES. DATE: 11-3-88. MAP NO: 8271-41.
 C. PETERSON ASSOCIATES. LINE: 11-3-89. MAP NO: 8271-41.
 D. "CONNECTICUT STATE HORMAY DEPARTMENT REAFT OF WAY MAP TOWN OF TOLLAND WILLWANTIC-STAFFORD SPRINGS ROAD FROM THE WILLINGTON TOWN LINE. N'LY TO THE ELLINGTON TOWN LINE. ROUTE NO. 32⁴ APROVED WILLUA J. COX. DATE: SEPT 30, 1940. REVISED CLEUSE C. MILE BLINGTON, CON'T BY GERKORIN & MARTELLI, CML ENGRS, DATE: NOVEMBER 1938.
 F. "RGHT OF WAY MAN THACK MAP NEW LONDON NORTHERN R.R. CO. OPERATED BY THE CENTRAL VERWONT RY. CO. STATION 2481+60 TO STATION 2534+40° BY THE OFFICE OF WALLMAND FROMERER 1358. RUMBER: 142-06. SHEET 1 OF 1.
 E.PROFERT OF ELER KOMERER 1358. RUMS EXAMON, SHEET V-148.
 G. "MAP PREPARED FOR PETER ROWN & HELDIN C. NOWAL STATFORD SPRINGS -WILLINATIC ROWERES RISK AND SEX MONDER SOLAWAY STAFFORD SPRINGS -WILLINATIC ROWERES RISK AND STATEMON TOWN AND THE OFFICE OF WALLAND BLINKTON, CON CT CONN. ROUTE \$25. DISONAWY MAP" BY WILLINATIC STAFFORD ELINGTON, CONTON THE 1983. NORTH AVERICAN DATUM (MAD
 S. BARGHT OW WAY AND THACK MAP NEW LONDON NORTHERN R.R. CO. OPERATED BY THE CENTRAL VERWONT RY. CO. STATION 2481+50 TO STATION 2534+40° BY THE OFFICE OF WALLINATIC ROWERES RISK. BALING SEXTON TO BOUNDANY MAP" BY WILLINATIC ROWSERS RIGHT AND STREMON TO THE 1983. NORTH AVERICAN DATUM (MAD
 S. BARGHT ON THIS PLAN ARE BASED ON THE 1983. NORTH AVERICAN DATUM (MAD
- BEARINGS DEPICTED ON THIS PLAN ARE BASED ON THE 1983 NORTH AMERICAN DATUM (NAD B3/87) BASED ON GPS COORDINATES PROVIDED BY SLR CONSULTING.
- 4. INLAND WETLANDS DEPICTED ON THIS PLAN WERE DELINEATED BY SLR CONSULTING





1"=100'

11-09-2022

3 OF 3

11075 A

E.R.P.



Property Information

Property ID	06/A/001
Location	343 PLAINS ROAD
Owner	GIRL SCOUTS CONN TRAILS COUNCIL



MAP FOR REFERENCE ONLY NOT A LEGAL DOCUMENT

Town of Tolland, CT makes no claims and no warranties, expressed or implied, concerning the validity or accuracy of the GIS data presented on this map.

Geometry updated October 25, 2021 Data updated daily Print map scale is approximate. Critical layout or measurement activities should not be done using this resource.

Map Theme Legends

Wetlands - Soils

Poorly Drained and Very Poorly Drained Soils Alluvial and Floodplain Soils

CT DEEP

Topography

× Spot Elevation
 ✓ Intermediate Contour
 ✓ Index Countour

Wetlands - Delineated

Delineated Wetlands

Topography 2016

— 100 ft

— 50 ft — 20 ft

— 10 ft

CT Eco Contours 2016



January 27, 2023

Ms. Diana Mahoney Chief Executive Officer Hartford Service Center 340 Washington Street Hartford, CT 06106

Re: Wetland Delineation Camp Yankee Trails – Phase 1 Detailed Design Girl Scouts of Connecticut Tolland, Connecticut SLR #141.13280.00006

Dear Ms. Mahoney,

On October 7, 2022, Matthew Sanford, Registered Soil Scientist and Professional Wetland Scientist, and Meaghan Fogarty, Environmental Scientist, both of SLR International Corporation (SLR) visited the Camp Yankee Trails site, located at 343 Plains Road in Tolland, Connecticut (**Figure 1**). The purpose of the site investigation was to determine the presence or absence of wetlands and/or watercourses and delineate boundaries of wetlands and watercourses, as defined by local, state, and federal statutes. Our investigation was limited to approximately 27 acres of the site's approximately 287-acre property, based on locations of proposed improvements. In summary, regulated resources within the study area consist of Sweetheart Lake, an adjacent forested wetland, an open water/emergent marsh wetland, and two isolated forested wetlands.

The subject site, a Girl Scouts of Connecticut camp, is located within a largely undeveloped portion of northeastern Tolland. It is accessible from the east via Plains Road and supports a number of buildings, including troop houses, a boathouse, and a dining hall. The New England Central railroad line is situated along the eastern property boundary. Approximately 200 feet off site to the east, the Willimantic River flows south between the railroad and River Road. Bonemill Brook, which flows east through the subject property, is impounded by an earthen dam at the eastern extent of Sweetheart Lake. A spillway conveys the watercourse east, where it flows for approximately 1,000 feet before draining into the Willimantic River. Topography on site generally slopes down from west to east, towards the Willimantic River. Approximate elevations within the study area range from 425 to 534 feet above mean sea level (MSL).

The site is located within the northern portion of the Willimantic River subregional watershed (basin #3100), which spans 51.2 square miles from Stafford to Windham. The Willimantic River flows south to its convergence with the Shetucket River in Windham before draining into the Thames River in Norwich. The



Thames River empties into the Long Island Sound in New London/Groton. According to the most recent Federal Emergency Management Agency (FEMA) mapping (effective April 1, 1982) no digital data is available regarding onsite flood hazards.

Wetland Delineation

Inland wetlands and watercourses within the project site were delineated in accordance with the regulations of the Town of Tolland, Connecticut, and the State of Connecticut Inland Wetlands and Watercourses Act, CGS 22a-36 through 45. State-regulated wetland areas consist of any of the soil types designated by the National Cooperative Soils Survey as poorly drained, very poorly drained, alluvial, or floodplain. Regulated watercourses consist of rivers; streams; brooks; waterways; lakes; ponds; marshes; swamps; bogs; and all other bodies of water, natural or artificial, vernal or intermittent, public or private, not regulated pursuant to Sections 22a-28 to 22a-35 inclusive (tidal wetlands). Intermittent watercourse determinations were made based on the presence of a defined permanent channel and bank and the occurrence of two or more of the following characteristics: A) evidence of scour or deposits of recent alluvium or detritus, B) the presence of standing or flowing water for a duration longer than a particular storm incident, and C) the presence of hydrophytic vegetation. On the day of the site investigation, weather conditions were sunny with an air temperature of approximately 65°F. Site conditions were suitable for wetland delineation work.

Inland wetland delineation methods followed the 1987 U.S. Army Corps of Engineers (USACE) *Wetlands Delineation Manual* (USACE, 1987) and *Regional Supplement to the Corps of Engineers Wetland Delineation Manual for the Northcentral and Northeast Region* (USACE, 2012). The classification system of the National Cooperative Soil Survey and Field Indicators of Hydric Soils in the United States (USDA, 2017) were used in this investigation. Soils were examined using a Dutch auger. Geospatial data was accessed via the United States Department of Agriculture – Natural Resources Conservation Service (USDA-NRCS) web soil survey mapping. The soil survey mapping is appended (**Figure 2**). The survey identifies the following soil mapping units with associated NRCS map numbers in the study area:

- Nipmuck-Brookfield complex, very rocky (72C & 72E) Well drained
- Fluvaquents-Udifluvents complex, frequently flooded (109) Poorly drained

In general, the soils observed within the project area were consistent with those mapped by the USDA-NRCS web soil survey. Please note that SLR did not fully delineate the upland soil types within the project area. Sequentially numbered flags delineating the boundary of the ordinary high water (OHW) line along the lake (blue) and state and federal wetlands (pink) were attached to sturdy vegetation within the study area and generally spaced every 30 to 50 feet; the locations were recorded using a handheld Global Positioning System (GPS) unit with submeter accuracy. The flag locations and numbers are depicted on the attached wetlands and watercourses map (**Figure 3**). Complete boundaries are located along the lines that



connect these sequentially numbered flags. The delineated wetland resources are described further below.

Sweetheart Lake/Bonemill Brook

The OHW boundary of Sweetheart Lake was delineated within the study area, represented by flags Ohw-1 through Ohw-62 (Figure 3). On the day of investigation, the lake's water surface elevation was significantly lower than its OHW, which can be attributed to the moderate to severe summer drought conditions affecting Connecticut this year. Bonemill Brook flows into the lake at its western extent. Two dock structures extend towards the center from the northern shore, and a riprap bar bisects the lake at its narrowest point to create a sediment forebay along its western shoreline. The earthen dam at the eastern extent contains a stone and concrete spillway, which conveys Bonemill Brook east through a triple-pipe culvert below Plains Road. The lake's substrate is comprised of silt, sand, and organic materials.

The lake is generally surrounded by upland forest, supporting a canopy of eastern white pine (*Pinus strobus*), eastern white oak (*Quercus alba*), black oak (*Quercus velutina*), northern red oak (*Quercus rubra*), sugar maple (*Acer saccharum*), and red maple (*Acer rubrum*). The margins of the lake, directly along its OHW line, support gray birch (*Betula populifolia*), black cherry (*Prunus serotina*), scrub oak (*Quercus ilicifolia*), alder (*Alnus sp.*), highbush blueberry (*Vaccinium corymbosum*), and mountain laurel (*Kalmia latifolia*). Below the OHW line, hydrophytic herbaceous vegetation has populated areas once inundated by the lake, including water purslane (*Ludwigia palustris*), rice cut grass (*Leersia oryzoides*), deer-tongue panicgrass (*Dichanthelium clandestinium*), straw-colored flatsedge (*Cyperus strigosus*), and jewelweed (*Impatiens capensis*). A small stand (approximately 20 stalks) of the highly invasive common reed (*Phragmites australis*) was observed along the northern shore of the lake, downgradient from the entry parking area. SLR recommends this stand be treated by the organization to help prevent its spread and further colonization of the lake shoreline.

Forested Wetlands

Four federal/state-regulated wetlands were delineated throughout the study area: one forested wetland adjacent to Sweetheart Lake (**Wetland A**), two isolated forested wetlands (**Wetland X and Y**), and one open water/emergent marsh wetland (**Wetland Z**).

Wetland A is a palustrine forested wetland adjacent to Sweetheart Lake, north of to the lake's northern finger, and bounded to the north, west, and east by a camp road. It is represented by flags Wa-1 through Wa-14 and abuts flags Ohw-28 through Ohw-31. The low-lying area is dominated by yellow birch (*Betula alleghaniensis*) and red maple, with an understory comprised of Japanese barberry (*Berberis thunbergii*), highbush blueberry, multiflora rose (*Rosa multiflora*), poison ivy (*Toxicodendron radicans*), sensitive fern (*Onoclea sensibilis*), cinnamon fern (*Osmundastrum cinnamomeum*), and sedges (*Carex sp.*). Stained leaves and drainage patterns confirmed persistent saturation.



Wetlands X and Y occur north of the dining hall and are represented by flags WX-1 through WX-6 and WY-1 through WY-11, respectively. They are both flat, isolated, palustrine forested wetlands supported by groundwater discharge. Stones, boulders, and microtopography throughout both wetlands contribute to their structural complexity. Neither possess a formal outlet; however, due to their geomorphic position and lack of appropriate hydrologic conditions, they are not classified as vernal pools. Both wetlands are dominated by red maple, highbush blueberry, American witch-hazel (*Hamamelis virginiana*), ferns, and sedges.

Wetland Z is a depressional system classified as palustrine open water wetland and emergent marsh. It is represented by flags WZ-1 through WZ-6 and is located in the northeast portion of the study area, north of Sweetheart Lake and just east of Plains Road. Please note, based on the defined study area, the entire boundary of this wetland system was not delineated. Vegetation along the shoreline is comprised primarily of red maple, sweet pepperbush (*Clethra alnifolia*), and highbush blueberry. The open water portion is dominated by buttonbush (*Cephalanthus occidentalis*), speckled alder (*Alnus incana*), and highbush blueberry. Herbaceous vegetation within this wetland is comprised of woolgrass (*Scirpus cyperinus*), soft rush (*Juncus effusus*), swamp beggar-ticks (*Bidens frondosa*), and sedges.

Functions and Values

SLR also assessed the study area's wetland systems based on functions and values that they perform within the localized/regional watershed, based on the USACE *Highway Methodology Workbook*. The primary functions and values of Sweetheart Lake and adjacent forested wetland (**Wetland A**) within the study area include the following:

- Recreation
- Sediment/toxicant retention
- Nutrient removal/retention/transformation
- Fish habitat
- Wildlife habitat
- Production export

The primary functions and values of the isolated forested wetland systems (**Wetlands X and Y**) within the study area include the following:

- Groundwater recharge/discharge
- Wildlife habitat (non-water dependent)

The primary functions and values of the open water/emergent marsh (**Wetland Z**) within the study area include the following:

- Sediment/toxicant retention
- Nutrient removal/retention/transformation
- Floodflow alternation
- Fish habitat
- Wildlife habitat

If you have any questions regarding this soil scientist report, please do not hesitate to contact either of the undersigned at (203) 271-1773.

Very truly yours,

SLR International Corporation

Manta

Matthew J. Sanford, MS, PWS US Manager of Ecology

Meaghan Fogarty Meaghan Fogarty

Environmental Scientist

Enclosures: Figures 1, 2, and 3 Photolog

13280.00006.j2723.ltr.docx

SI RC





USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey

	MAP L	EGEND		MAP INFORMATION
Area of In Soils	terest (AOI) Area of Interest (AOI) Soil Map Unit Polygons	8 0 00 1 1 1	Spoil Area Stony Spot Very Stony Spot Wet Spot	The soil surveys that comprise your AOI were mapped at 1:12,000. Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause
Special	Soil Map Unit Points Point Features Planaut	∆ •• Water Feat	Other Special Line Features ures	line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.
> ☆ * * * * * * * * * * * * * * * * * *	Blowout Borrow Pit Clay Spot Closed Depression Gravel Pit Gravelly Spot Landfill Lava Flow Marsh or swamp Mine or Quarry Miscellaneous Water Perennial Water Rock Outcrop Saline Spot Sandy Spot Severely Eroded Spot	Water Feat	streams and Canals ttion Rails Interstate Highways US Routes Major Roads Local Roads d Aerial Photography	 Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: State of Connecticut Survey Area Data: Version 22, Sep 12, 2022 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Sep 3, 2019—Oct 22, 2019 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
ل ب ا	Sinkhole Slide or Slip Sodic Spot			imagery displayed on these maps. shifting of map unit boundaries ma



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
72C	Nipmuck-Brookfield complex, 3 to 15 percent slopes, very rocky	9.8	38.8%
72E	Nipmuck-Brookfield complex, 15 to 45 percent slopes, very rocky	7.1	28.3%
109	Fluvaquents-Udifluvents complex, frequently flooded	3.5	14.0%
W	Water	4.8	19.0%
Totals for Area of Interest		25.1	100.0%





Photo No. Date: 2 10/7/22 Direction Photo Taken: West Taken: West Sweatheart Description: Sweetheart Lake from its northwestern shore. Note the distinct break in slope

Sweetheart Lake from its northwestern shore. Note the distinct break in slope and line of perennial vegetation indicating the ordinary high water line.











PHOTOGRAPHIC LOG

Client Name: Girl Scouts of Connecticut

Photo No.Date:910/7/22Direction Photo Taken:East

Description: Wetland X – Isolated Forested Wetland



Photo No.Date:1010/7/22Direction Photo Taken:West

Description: Wetland Y – Isolated Forested Wetland



尜SLR

Camp Yankee Trails Site Improvements

343 Plains Road Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

20 Washington Avenue North Haven, CT 06473

Prepared by:

SLR International Corporation

99 Realty Drive, Cheshire, Connecticut, 06410

SLR Project No.: 141.13280.00006.0080

November 20, 2023



Making Sustainability Happen

Drainage Report

Camp Yankee Trails Site Improvements 343 Plains Road Tolland, Connecticut SLR #141.13280.000006.0080

This Drainage Report has been prepared in support of the proposed upgrades to the existing Girl Scouts camp on Plains Road in the town of Tolland, Connecticut. This project includes renovations and additions to the dining hall, a new shower house, and four new cabins including an Americans with Disabilities Act (ADA) accessible unit, a new parking lot, stone dust and concrete paths, an access road, and stormwater improvements.



Figure 1 – 343 Plains Road, Map, Block, Lot (MBL): 06-A-001



Table 1 – Stormwater Data

Parcel Size Total	221 acres
Existing Impervious Area (Watershed Area)	0.74 acres
Proposed Impervious Area (Watershed Area)	1.79 acres
Soil Type (Hydrologic Soil Group)	"B" and "C"
Existing Land Use	Open space, woods, gravel, water, building, and paved/impervious cover
Proposed Land Use	Open space, woods, gravel, water, building, and paved/impervious cover
Design Storm for Stormwater Management	No increases in peak rates of runoff for the 2-, 10-, 25-, 50-, and 100-year storms; Connecticut Department of Energy & Environmental Protection (CTDEEP) water quality volume (WQV)
Water Quality Measures	Catch basins with 2-foot sumps, underground detention system, and retention/infiltration storage for WQV
Design Storm for Storm Drainage	25-year storm
Federal Emergency Management Agency (FEMA) Special Flood Hazard Areas	Area of Minimal Flood Hazard (Zone X)
Connecticut Department of Energy & Environmental Protection Aquifer Protection Areas	None

Stormwater Management Approach

The proposed stormwater management system for the project focuses on providing water quality management while attenuating proposed peak flows. Water quality treatment in accordance with the CTDEEP requirements for WQV is provided. The proposed stormwater treatment train consists of catch basins with 2-foot sumps and retention/infiltrations storage for the WQV.

The computer program entitled *Hydraflow Storm Sewers Extension for AutoCAD*[®] *Civil 3D*[®] *2023* by Autodesk, Inc. was used for designing the proposed storm drainage collection system. Storm drainage computations performed include pipe capacity and hydraulic grade line calculations. The contributing watershed to each individual catch basin inlet was delineated to determine the drainage area and land coverage. These values were used to determine the stormwater runoff to each inlet using the Rational Method. The rainfall intensities for the site were obtained from the National Oceanic and Atmospheric Administration (NOAA) Atlas 14,



Volume 10, Precipitation Frequency Data Server (PFDS). The proposed storm drainage system is designed to provide adequate capacity to convey the 25-year storm event.

Water Quality Management

Water quality measures or Best Management Practices (BMPs) have been incorporated into the design to maintain water quality to provide protection of the areas downgradient of the proposed development. The proposed stormwater management system will include catch basins with 2-foot sumps and retention/infiltration storage for the WQV.

The proposed stormwater basin will provide retention volume along its bottom, thus creating a water quality feature within it. This serves several purposes, including stormwater renovation and first-flush retention. The vegetation will provide pollutant removal by filtering stormwater runoff and utilizing excess nutrients that may be present in the stormwater. The CTDEEP *2004 Stormwater Quality Manual* (Chapter 7) recommends methods for sizing stormwater treatment measures with WQV computations. The WQV addresses the initial stormwater runoff, also commonly referred to as the "first-flush" runoff. The WQV provides adequate volume to store the runoff associated with the first 1 inch of rainfall, which tends to contain the highest concentration of potential pollutants. Supporting calculations have been included in the Appendix of this report.

Hydrologic Analysis

A hydrologic analysis was conducted to analyze the predevelopment and postdevelopment peak-flow rates from the site. One analysis point was selected, as it receives all runoff from the site. Analysis Point A represents Sweetheart Lake. The total watershed area delineated is approximately 46.6 acres under both existing and proposed conditions.

The method of predicting the surface water runoff rates utilized in this analysis was a computer program titled *Hydraflow Hydrographs Extension for AutoCAD*[®] *Civil 3D*[®] *2019* by Autodesk, Inc., Version 2020. The *Hydrographs* program is a computer model that utilizes the methodologies set forth in the *Technical Release No. 55* (TR-55) manual and *Technical Release No. 20* (TR-20) computer model, originally developed by the United States Department of Agriculture – Natural Resources Conservation Service (USDA-NRCS). The *Hydrographs* computer modeling program is primarily used for conducting hydrology studies such as this one.

The *Hydrographs* computer program forecasts the rate of surface water runoff based upon several factors. The input data includes information on land use, hydrologic soil type, vegetation, contributing watershed area, time of concentration, rainfall data, storage volumes, and the hydraulic capacity of structures. The computer model predicts the amount of runoff as a function of time, with the ability to include the attenuation effect due to dams, lakes, large wetlands, floodplains, and stormwater management basins. The input data for rainfalls with statistical recurrence frequencies of 2, 10, 25, 50, and 100 years was obtained from the NOAA Atlas 14, Volume 10 database. The corresponding rainfall totals are listed below.

Storm Frequency	Rainfall (inches)
2-year	3.25
10-year	5.07
25-year	6.21
50-year	7.04
100-year	7.96



Land use for the site under existing and proposed conditions was determined from field survey and aerial photogrammetry. Land use types used in the analysis included grassed or open space, woods, water, gravel, building, and impervious (paved) cover. Soil types in the watershed were determined from the CTDEEP Geographic Information System (GIS) database of the USDA-NRCS soil survey for Tolland County, Connecticut. For the analysis, the site was determined to contain hydrologic soil types "B" and "C" as classified by USDA-NRCS. Composite runoff Curve Numbers (CN) for each subwatershed were calculated based on the different land use and soil types. The time of concentration (Tc) was estimated for each subwatershed using the TR-55 methodology and was computed by summing all travel times through the watershed as sheet flow, shallow concentrated flow, and channel flow.

The existing conditions were modeled with the *Hydrographs* program to determine the peak-flow rates for the various storm events at the analysis point. A revised model was developed incorporating the proposed site conditions, the underground chamber system, and the stormwater management basin. The flows obtained with the revised model were then compared to the results of the existing conditions model. Peak-flow rates from the project site were controlled by the storage volume provided within the stormwater management basin and the underground chamber system.

Analysis Point A – Sweetheart Lake					
	Peak Runoff Rate (cubic feet per second)				
Storm Frequency (years)	2 10 25 50 100				
Existing Conditions	7.7	37.0	61.7	81.4	104.6
Proposed Conditions	7.5	35.7	60.8	81.0	104.2

The following peak rates of runoff were obtained from the *Hydrographs* hydrology results:

Detention Basin 110*					
	Water Surface Elevation (feet)				
Storm Frequency (years)	2 10 25 50 100				100
Proposed Conditions	448.4	448.9	449.2	449.3	449.4

*Top of Berm Elevation = 450.3

Underground Chamber System 111**					
	Water Surface Elevation (feet)				
Storm Frequency (years) 2 10 25 50 100					100
Proposed Conditions	441.5	443.1	443.7	444.1	444.8

**Top of Stone Elevation = 445.0



Conclusion

The results of the hydrologic analysis demonstrate that there will be no increases in peak-flow rates from the proposed development. This was achieved for storm events modeled through a planned stormwater management system with a subsurface infiltration system and stormwater management basin. The proposed development will also introduce a new stormwater treatment train consisting of catch basins with 2-foot sumps and retention/infiltration of the WQV.

All supporting documentation and stormwater-related computations are attached to this report along with the *Hydrographs* model results for stormwater management and *Hydraflow Storm Sewers* model results for the proposed storm drainage system. Illustrative watershed maps for both existing and proposed conditions are also attached to this report.

Appendices

Appendix A United States Geological Survey Location Map Appendix B Federal Emergency Management Agency Flood Insurance Rate Map Appendix C Natural Resources Conservation Service Hydrologic Soil Group Map Appendix D Storm Drainage Computations Appendix E Water Quality Computations Appendix F Hydrologic Analysis – Existing Conditions Hydrologic Analysis – Proposed Conditions Appendix G Watershed Maps Appendix H

13280.00006.0080.n2023.rpt.docx





Appendix A United States Geological Survey Location Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023







Appendix B FEMA Flood Insurance Rate Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023







Appendix C Natural Resources Conservation Service Hydrologic Soil Group Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023





National Cooperative Soil Survey

Conservation Service

8/24/2**623** Page 1 of 4



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at

Please rely on the bar scale on each map sheet for map

Source of Map: Natural Resources Conservation Service Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut Survey Area Data: Version 22, Sep 12, 2022

Soil map units are labeled (as space allows) for map scales

Date(s) aerial images were photographed: Jun 14, 2022-Oct 6,

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	1.8	0.6%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	B/D	0.0	0.0%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	В	42.9	15.2%
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	В	8.4	3.0%
71C	Nipmuck-Brimfield-Rock outcrop complex, 3 to 15 percent slopes	В	17.4	6.2%
71E	Nipmuck-Brimfield-Rock outcrop complex, 15 to 45 percent slopes	В	47.9	17.0%
72C	Nipmuck-Brookfield complex, 3 to 15 percent slopes, very rocky	В	33.5	11.9%
72E	Nipmuck-Brookfield complex, 15 to 45 percent slopes, very rocky	В	40.5	14.4%
85C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes, very stony	С	35.3	12.5%
109	Fluvaquents-Udifluvents complex, frequently flooded	B/D	39.6	14.1%
W	Water		14.2	5.0%
Totals for Area of Inter	rest		281.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



Appendix D Storm Drainage Computations

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023


Project: Location:	Camp Yankee ⁻ 343 Plains Roa	Trails Site Imp d, Tolland, CT	rovement		By: Checked:	JLS MCB	Date: Date:	11/16/23 11/17/23
Basin Name	Impervious Area C=0.9 (sf)	Grassed Area C=0.3 (sf)	Gravel Area C=0.6 (sf)	Wooded Area C=0.2 (sf)	Total Area (sf)	Total Area (ac)	Weighted C	Tc (min)
		X- 4	Sys	stem 110				
MH 5	907	848	0	32	1787	0.04	0.60	5.0
MH 6	2207	6311	512	6753	15783	0.36	0.35	5.0
MH 7	5492	5055	0	9041	19588	0.45	0.42	5.0
MH 8	3270	3165	0	0	6435	0.15	0.60	5.0
MH 9	1793	1899	219	294	4205	0.10	0.56	5.0
MH 10	969	535	0	0	1504	0.03	0.69	5.0
CLCB 11	11775	3336	0	0	15111	0.35	0.77	5.0
CLCB 12	7651	5971	0	0	13622	0.31	0.64	5.0
YD 13	432	392	0	0	824	0.02	0.61	5.0
CLCB 14	1881	347	0	0	2228	0.05	0.81	5.0
YD 15	818	343	0	0	1161	0.03	0.72	5.0
YD 16	0	603	0	0	603	0.01	0.30	5.0

Storm Sewer IDF Curves



Storm Sewers



NOAA Atlas 14, Volume 10, Version 3 Location name: Tolland, Connecticut, USA* Latitude: 41.9274°, Longitude: -72.3121° Elevation: 579 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	ased poir	nt precipit	ation freq	luency es	timates w	ith 90% c	onfidence	intervals	(in inches	s/hour) ¹
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	4.02 (3.06-5.27)	4.82 (3.67-6.32)	6.13 (4.67-8.09)	7.22 (5.46-9.55)	8.72 (6.41-12.0)	9.85 (7.12-13.9)	11.0 (7.75-16.1)	12.3 (8.26-18.4)	14.2 (9.17-21.9)	15.7 (9.91-24.7)
10-min	2.84 (2.17-3.73)	3.41 (2.60-4.48)	4.34 (3.30-5.72)	5.12 (3.87-6.77)	6.18 (4.54-8.52)	6.98 (5.03-9.82)	7.81 (5.49-11.4)	8.73 (5.84-13.0)	10.0 (6.49-15.5)	11.1 (7.02-17.5)
15-min	2.23 (1.70-2.92)	2.68 (2.04-3.51)	3.40 (2.59-4.48)	4.01 (3.04-5.30)	4.84 (3.56-6.68)	5.47 (3.94-7.70)	6.13 (4.30-8.93)	6.85 (4.59-10.2)	7.87 (5.09-12.2)	8.70 (5.51-13.7)
30-min	1.51 (1.15-1.98)	1.82 (1.38-2.38)	2.31 (1.76-3.04)	2.72 (2.06-3.60)	3.29 (2.42-4.54)	3.72 (2.68-5.23)	4.16 (2.92-6.07)	4.65 (3.12-6.94)	5.35 (3.46-8.26)	5.91 (3.74-9.31)
60-min	0.954 (0.729-1.25)	1.15 (0.874-1.50)	1.46 (1.11-1.92)	1.72 (1.30-2.28)	2.08 (1.53-2.87)	2.35 (1.69-3.30)	2.63 (1.85-3.83)	2.94 (1.97-4.39)	3.38 (2.19-5.22)	3.74 (2.37-5.88)
2-hr	0.609 (0.467-0.794)	0.730 (0.559-0.952)	0.927 (0.707-1.21)	1.09 (0.828-1.43)	1.32 (0.972-1.81)	1.48 (1.08-2.09)	1.66 (1.18-2.43)	1.87 (1.26-2.78)	2.18 (1.42-3.36)	2.45 (1.55-3.83)
3-hr	0.467 (0.358-0.606)	0.559 (0.429-0.727)	0.711 (0.544-0.927)	0.837 (0.637-1.10)	1.01 (0.749-1.39)	1.14 (0.831-1.60)	1.28 (0.912-1.87)	1.44 (0.971-2.14)	1.70 (1.10-2.60)	1.92 (1.22-2.99)
6-hr	0.296 (0.229-0.383)	0.358 (0.276-0.462)	0.457 (0.351-0.593)	0.540 (0.413-0.704)	0.654 (0.488-0.895)	0.738 (0.541-1.03)	0.829 (0.597-1.21)	0.943 (0.636-1.39)	1.12 (0.728-1.70)	1.27 (0.811-1.97)
12-hr	0.184 (0.143-0.236)	0.224 (0.173-0.288)	0.290 (0.223-0.374)	0.344 (0.264-0.446)	0.419 (0.314-0.570)	0.474 (0.349-0.661)	0.534 (0.386-0.777)	0.609 (0.412-0.891)	0.726 (0.474-1.10)	0.828 (0.529-1.28)
24-hr	0.110 (0.085-0.140)	0.135 (0.105-0.173)	0.177 (0.137-0.226)	0.211 (0.163-0.272)	0.258 (0.194-0.350)	0.293 (0.217-0.407)	0.331 (0.241-0.480)	0.379 (0.257-0.552)	0.454 (0.298-0.683)	0.520 (0.334-0.797)
2-day	0.062 (0.048-0.079)	0.077 (0.060-0.098)	0.102 (0.079-0.130)	0.122 (0.094-0.156)	0.150 (0.113-0.203)	0.171 (0.127-0.236)	0.193 (0.141-0.280)	0.222 (0.151-0.322)	0.268 (0.176-0.401)	0.309 (0.199-0.470)
3-day	0.045 (0.035-0.057)	0.056 (0.044-0.071)	0.074 (0.057-0.094)	0.088 (0.069-0.113)	0.109 (0.082-0.147)	0.124 (0.092-0.171)	0.140 (0.103-0.202)	0.161 (0.110-0.233)	0.195 (0.128-0.291)	0.225 (0.145-0.341)
4-day	0.036 (0.028-0.045)	0.045 (0.035-0.056)	0.059 (0.046-0.075)	0.071 (0.055-0.090)	0.087 (0.066-0.117)	0.099 (0.074-0.136)	0.112 (0.082-0.161)	0.129 (0.088-0.186)	0.156 (0.103-0.232)	0.180 (0.116-0.272)
7-day	0.024 (0.019-0.030)	0.030 (0.023-0.038)	0.039 (0.031-0.049)	0.047 (0.036-0.059)	0.057 (0.043-0.076)	0.065 (0.049-0.089)	0.073 (0.054-0.105)	0.084 (0.058-0.121)	0.101 (0.067-0.150)	0.117 (0.075-0.176)
10-day	0.019 (0.015-0.025)	0.024 (0.019-0.030)	0.031 (0.024-0.039)	0.036 (0.028-0.046)	0.044 (0.034-0.059)	0.050 (0.037-0.068)	0.056 (0.041-0.080)	0.064 (0.044-0.092)	0.076 (0.050-0.113)	0.087 (0.056-0.131)
20-day	0.014 (0.011-0.017)	0.016 (0.013-0.020)	0.020 (0.015-0.025)	0.023 (0.018-0.029)	0.027 (0.020-0.035)	0.030 (0.022-0.040)	0.033 (0.024-0.047)	0.037 (0.026-0.053)	0.043 (0.028-0.063)	0.048 (0.031-0.071)
30-day	0.011 (0.009-0.014)	0.013 (0.010-0.016)	0.016 (0.012-0.019)	0.018 (0.014-0.022)	0.020 (0.015-0.027)	0.023 (0.017-0.030)	0.025 (0.018-0.034)	0.027 (0.019-0.038)	0.030 (0.020-0.045)	0.033 (0.021-0.049)
45-day	0.010 (0.007-0.012)	0.011 (0.008-0.013)	0.012 (0.010-0.015)	0.014 (0.011-0.017)	0.016 (0.012-0.020)	0.017 (0.013-0.023)	0.019 (0.013-0.025)	0.020 (0.014-0.028)	0.022 (0.015-0.032)	0.023 (0.015-0.035)
60-day	0.008 (0.007-0.010)	0.009 (0.007-0.011)	0.010 (0.008-0.013)	0.011 (0.009-0.014)	0.013 (0.010-0.017)	0.014 (0.010-0.019)	0.015 (0.011-0.021)	0.016 (0.011-0.023)	0.017 (0.012-0.025)	0.018 (0.012-0.027)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top



PDS-based intensity-duration-frequency (IDF) curves Latitude: 41.9274°, Longitude: -72.3121°





NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Thu Aug 24 13:11:05 2023

Back to Top

Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Inventory Report

Line		Align	ment			Flow	Data					Physical	Data			Line ID	
NO.	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	61	-13	Grate	0.00	0.36	0.35	5.0	445.00	4.10	447.50	12	Cir	0.012	1.50	452.50	OUTFALL - MH 6
2	1	78	-103	Grate	0.00	0.04	0.60	5.0	449.20	10.00	457.00	12	Cir	0.012	1.23	461.00	MH 6 - MH 5
3	2	47	52	Grate	0.00	0.45	0.42	5.0	458.20	10.00	462.90	12	Cir	0.012	0.51	469.50	MH 5 - MH 7
4	3	99	17	Grate	0.00	0.15	0.60	5.0	466.50	8.28	474.70	12	Cir	0.012	0.92	477.70	MH 7 - MH 8
5	4	133	-34	Grate	0.00	0.10	0.56	5.0	474.70	6.62	483.50	12	Cir	0.012	0.81	488.50	MH 8 - MH 9
6	5	78	-29	Grate	0.00	0.03	0.69	5.0	485.50	9.87	493.20	12	Cir	0.012	1.33	499.44	MH 9 - MH 10
7	6	59	-2	Grate	0.00	0.05	0.81	5.0	495.50	10.17	501.50	12	Cir	0.012	1.32	505.00	MH 10 - CLCB 14
8	7	34	-59	DrGrt	0.00	0.03	0.72	5.0	502.00	3.53	503.20	12	Cir	0.012	1.37	506.20	CLCB 14 - YD 15
9	8	66	63	DrGrt	0.00	0.01	0.30	5.0	503.70	3.18	505.80	8	Cir	0.012	1.00	508.30	YD 15 - YD 16
10	6	41	-60	Grate	0.00	0.35	0.77	5.0	495.50	9.76	499.50	12	Cir	0.012	0.81	504.00	MH 10 - CLCB 11
11	10	122	-29	Grate	0.00	0.31	0.64	5.0	501.00	1.64	503.00	12	Cir	0.012	1.50	506.00	CLCB 11 - CLCB 12
12	11	47	94	DrGrt	0.00	0.02	0.61	5.0	503.00	2.13	504.00	12	Cir	0.012	1.00	507.00	CLCB 12 - YD 13
Project	File: Syst	em 110.stn	n									Number c	of lines: 12			Date: 1	1/17/2023

80 Storm Sewers v2023.00

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	с	Тс		Rain	Total	Cap	Vel	Pipe		Invert El	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
Line	To		Incr	Total	coen	Incr	Total	Inlet	Syst		now	Tun		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	Final	C1	0.00	1.00	0.25	0.12	1.05	5.0		7.4	7 00	7.01	0.04	10	4.10	445.00	447.50	110.10	454.00	447.00	452.50	
	End		0.36	1.90	0.35	0.13	1.05	5.0		7.4	7.00	12.20	9.94	12	4.10	445.00	447.50	449.10	451.60	447.30	452.50	
2	2	10	0.04	1.54	0.00	0.02	0.92	5.0	6.9	7.5	6.78	12.20	12.33	12	10.00	449.20	457.00	453.90	457.97	452.50	401.00	
1	2	47	0.45	1.50	0.42	0.19	0.90	5.0	6.8	7.5	5.42	11 10	10.57	12	8.28	450.20	402.90	450.75	403.07	401.00	409.50	
5	4	133	0.10	0.90	0.56	0.06	0.71	5.0	6.4	7.0	4 85	9.92	6.41	12	6.62	474 70	483.50	475.64	484 41	477 70	488.50	MH 8 - MH 9
6	5	78	0.03	0.80	0.69	0.02	0.57	5.0	6.3	7.0	4 4 5	12 12	10.16	12	9.87	485 50	493.20	485.92	494.08	488.50	499 44	MH 9 - MH 10
7	6	59	0.05	0.09	0.81	0.04	0.07	5.0	5.8	8.1	0.53	12.30	5.22	12	10.17	495.50	501.50	495.64	501.80	499.44	505.00	MH 10 - CLCB 14
8	7	34	0.03	0.04	0.72	0.02	0.02	5.0	5.6	8.3	0.20	7.25	3.04	12	3.53	502.00	503.20	502.12	503.38	505.00	506.20	CLCB 14 - YD 15
9	8	66	0.01	0.01	0.30	0.00	0.00	5.0	5.0	8.7	0.03	2.33	1.74	8	3.18	503.70	505.80	503.75	505.87	506.20	508.30	YD 15 - YD 16
10	6	41	0.35	0.68	0.77	0.27	0.48	5.0	6.2	7.9	3.80	12.05	9.52	12	9.76	495.50	499.50	495.89	500.33	499.44	504.00	MH 10 - CLCB 11
11	10	122	0.31	0.33	0.64	0.20	0.21	5.0	5.8	8.2	1.72	4.94	4.77	12	1.64	501.00	503.00	501.41	503.56	504.00	506.00	CLCB 11 - CLCB
12	11	47	0.02	0.02	0.61	0.01	0.01	5.0	5.0	8.7	0.11	5.63	0.97	12	2.13	503.00	504.00	503.56	504.13	506.00	507.00	CLCB 12 - YD 13
Proje	ct File:	System	110.stn	n												Numbe	r of lines: 1	2		Run Da	te: 11/17/2	2023
NOT	ES:Inte	nsity = 4	1.75 / (li	nlet time	+ 3.80)	^ 0.72; F	Return p	eriod =Y	′rs. 25;	c = cir e	e = ellip	b = box										

Hydraulic Grade Line Computations

Line	Size	Q					Len				Upsti	eam				Chec	k	JL	Minor				
			Invert elev	HGL	Depth	Area	Vel	Vel head	EGL elev	Sf		Invert elev	HGL	Depth	Area	Vel	Vel head	EGL	Sf	Ave Sf	Enrgy	соеп	IOSS
	(in)	(cfs)	(ft)	(ft)	(ft)	(sqft)	(ft/s)	(ft)	(ft)	(%)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft/s)	(ft)	(ft)	(%)	(%)	(ft)	(K)	(ft)
1	12	7.80	445.00	449.10	1.00	0.79	9.94	1.54	450.64	4.093	61	447.50	451.60	1.00	0.79	9.94	1.53	453.13	4.091	4.092	2.496	1.50	2.30
2	12	6.93	449.20	453.90	1.00	0.78	8.83	1.21	455.11	3.232	78	457.00	457.97 j	0.97**	0.78	8.89	1.23	459.20	2.861	3.047	n/a	1.23	n/a
3	12	6.78	458.20	458.73	0.53*	0.43	15.94	1.18	459.91	0.000	47	462.90	463.87	0.97**	0.78	8.71	1.18	465.05	0.000	0.000	n/a	0.51	0.60
4	12	5.42	466.50	466.99	0.49*	0.39	14.04	0.78	467.77	0.000	99	474.70	475.64	0.94**	0.76	7.09	0.78	476.42	0.000	0.000	n/a	0.92	n/a
5	12	4.85	474.70	475.64	0.94	0.75	6.34	0.65	476.29	0.000	133	483.50	484.41 j	0.91**	0.75	6.47	0.65	485.06	0.000	0.000	n/a	0.81	0.53
6	12	4.45	485.50	485.92	0.42*	0.31	14.24	0.57	486.49	0.000	78	493.20	494.08	0.88**	0.73	6.07	0.57	494.65	0.000	0.000	n/a	1.33	0.76
7	12	0.53	495.50	495.64	0.14*	0.07	7.80	0.11	495.75	0.000	59	501.50	501.80	0.30**	0.20	2.65	0.11	501.91	0.000	0.000	n/a	1.32	n/a
8	12	0.20	502.00	502.12	0.12*	0.05	4.04	0.06	502.18	0.000	34	503.20	503.38	0.18**	0.10	2.04	0.06	503.45	0.000	0.000	n/a	1.37	0.09
9	8	0.03	503.70	503.75	0.05*	0.01	2.22	0.02	503.77	0.000	66	505.80	505.87	0.07**	0.02	1.26	0.02	505.90	0.000	0.000	n/a	1.00	0.02
10	12	3.80	495.50	495.89	0.39*	0.28	13.59	0.46	496.35	0.000	41	499.50	500.33	0.83**	0.70	5.46	0.46	500.79	0.000	0.000	n/a	0.81	0.38
11	12	1.72	501.00	501.41	0.41*	0.30	5.72	0.23	501.63	0.000	122	503.00	503.56	0.56**	0.45	3.82	0.23	503.78	0.000	0.000	n/a	1.50	0.34
12	12	0.11	503.00	503.56	0.56	0.06	0.24	0.05	503.60	0.000	47	504.00	504.13 j	0.13**	0.06	1.71	0.05	504.18	0.000	0.000	n/a	1.00	0.05
Pr	oject File:	System	110.stm											N	umber c	f lines: 1	2		Rur	n Date:	11/17/20	23	
No	otes: * dep	oth assu	med; ** Criti	cal depth.;	j-Line co	ontains h	ıyd. jump	; c = ci	ir e = ellip	b = box													

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Inventory Report

Line		Align	ment			Flow	Data					Physical	Data				Line ID
NO.	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	49.000	-76.000	None	11.80	0.00	0.00	0.0	442.00	9.39	446.60	12	Cir	0.012	1.00	449.00	MH 3 - OCS 110
2	End	40.000	-109.000	рмн	4.27	0.00	0.00	0.0	441.00	5.00	443.00	12	Cir	0.012	1.00	446.40	OUTFALL - MH 2
Project	File: Syste	em 120.stm	ו									Number o	f lines: 2			Date: 1	1/17/2023

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	с	Tc		Rain	Total	Cap	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
Line	To Line		Incr	Total	-coen	Incr	Total	Inlet	Syst		now	Tun		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	49.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	11.80	11.82	15.03	12	9.39	442.00	446.60	449.30	453.89	447.00	449.00	MH 3 - OCS 110
2	End	40.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	4.27	8.63	5.66	12	5.00	441.00	443.00	442.00	443.87	442.10	446.40	OUTFALL - MH 2
Proje	ct File:	System	i 120.stn	n	<u> </u>		1		1	I	1	1	1	<u> </u>	I	Number of lines: 2 Run Date: 11/17/2023						
NOT	ES:Inte	nsity = 5	52.80 / (I	nlet time	e + 3.80)	^ 0.72; I	Return p	eriod =Y	′rs. 100	; c = cir	e = elli	p b=bo	x			1						
																					8	5

ÖQorm Sewers v2023.00

Hydraulic Grade Line Computations

L	ne Size Q Downstream											Len				Upstr	eam				Chec	k	JL	Minor
		(in)	(cfs)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	(ft)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy Ioss (ft)	(K)	(ft)
	1	10	11.00	142.00	140.20	1.00	0.70	15.02	2.54	450.04	0.250	40.000	140.00	452.00	1 00**	0.70	15.00	2.54	457.40	0.255	0.257	4 5 9 5	1.00	2.54
	2	12	4.27	442.00	449.30	1.00*	0.79	5.44	0.46	452.61	1.225	49.000	446.60	453.69 443.87 j	0.87**	0.79	5.89	0.54	457.40	1.119	9.357	4.565 n/a	1.00	n/a
	Proje	ect File: S	System 1	20.stm											N	lumber o	t lines: 2			Run	Date: 1	1/17/20	23	
	Note	s: * depth	n assum	ed; ** Criti	cal depth.;	j-Line cc	ontains h	yd. jump	; c = ci	r e = ellip	b = box											86。	torm Sawo	re v2023 0

Outlet	Protection	Calculations
		-

<u>Project:</u> <u>Location:</u> Outlet I.D.	Camp Yankee Trails 343 Plains Road, Tol <u>FES 1</u>	Site Im Iand, C	provement onnecticut	<u>By:</u> JLS <u>Checked:</u> MCB	<u>Date:</u> <u>Date:</u>	11/17/23 11/17/23
*Based on	Connecticut DOT Drain	age Ma	nual, Section 11.	13		
Description FES 1	<u>n:</u>					
<u>Design Cri</u>	teria (100-yr Storm Ev	<u>vent):</u>				
Q (cts)	= 4.27	$R_p(\pi) =$	1			
D (III) =	= 5.66	3 _p (it) – Tw (ft)=	: 1			
v (ipo)	0.00	· • • (it)	•			
Q= Flov	w rate at discharge poir	nt in cub	oic feet per second	d (cfs)		
D= Out	let pipe diameter (in)	: 1 / f t	(-)			
V= Flov R_= Ma	v velocity at discharge p Iximum inside pipe rise	201nt (11. <i>(</i> ff)	(S)			
S _p = ins	ide diametere for circula	ar sectio	ons of maximum i	nside pipe span for non	-circular	sections (ft)
T _w = Tai	ilwater depth (ft)					
Based on	Table 11-13.1 u	se Type	e 'B'> TW≥ 0.5	Rp		
Rip Rap St	one Size:					
Velocity	<u>Rip Rap Specif</u>	ication		D ₅₀ Stone Size		
0-8 fp	s Modified			5 inches		
Droformod	Coour Hole Dimonoio					
F(ft)=0.	5(R ₂)	<u>= = 0000000000000000000000000000000000</u>	n/a			
C(ft)=3.	.0(S _p)+6.0(F)	=	n/a			
B(ft)=2.	.0(S _p)+6.0(F)	=	n/a			
Din Don Su	leah Red Dimensions					
Rip Rap Sp	olash Pad Dimensions	<u>s:</u> =	10	ft		
<mark>Rip Rap Sp</mark> L _a W1 = 3	olash Pad Dimensions .0(Տր) min.	<u>8:</u> = =	10 3	ft ft		
Rip Rap Sr L _a W1 = 3 W2 = 3	olash Pad Dimensions .0(S _p) min. .0(Sp)+0.4(La) min.	<u>s:</u> = = =	10 3 7	ft ft ft		
Rip Rap Sr L _a W1 = 3 W2 = 3 d (Dept	<mark>blash Pad Dimensions</mark> .0(S _p) min. .0(Sp)+0.4(La) min. th of Stone)	<u>s:</u> = = =	10 3 7 12	ft ft inches		



	<u>_O</u> ı	utlet Protection Calcu	lations		
<u>Project:</u> Location: Outlet I.D.	Camp Yankee Tra 343 Plains Road, ⁻ <u>FES 5</u>	ils Site Improvement Tolland, Connecticut	<u>By:</u> JLS <u>Checked:</u> <u>MCB</u>	<u>Date:</u> <u>Date:</u>	11/17/2023 11/17/2023
*Based on (Connecticut DOT Dr	ainage Manual, Section 11.13	3		
Description FES 5	<u>ı:</u>				
Design Crit	eria (25-yr Storm E	Event):			
Q (cfs)	= 7.8	$R_{p}(ft)=$	1		
D (in) =	12	$S_{p}(ft) =$	1		
V (fps) :	= 9.94	Tw (ft)=	4.1		
V = Flow $R_p = Ma:$ $S_p = insi$ $T_w = Tai$ <u>Based on Ta</u> Rip Rap St e	v velocity at discharg ximum inside pipe ri de diametere for cirv water depth (ft) able 11.13.1, A Prei one Size:	, ge point (ft/s) se (ft) cular sections of maximum in <u>formed Scour Hole</u> is used O	side pipe span for non-ci <u>ne Half Pipe Rise Depre</u>	ircular se ssion (Ty	ctions (ft) <u>⁄pe /)</u>
D ₅₀ Con	nputed (ft)	Rip Rap Specification	D ₅₀ Stone Size Require	ed	
0.047	·····	Modified	5 inches		
Preformed F = 0.5(C = 3.0(B = 2.0(d (Dept	<u>Scour Hole Dimen</u> R _p) (S _p)+6.0(F) (S _p)+6.0(F) h of Stone)	<u>sions:</u> = = = =	0.5 ft 6ft 5ft 12 inches		









Appendix E Water Quality Computations

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023



STORMWATER QUALITY CALCULATIONS Water Quality Volume (WQV)

Basin	Total	Impervious	Percent	Volumetric	WQV	Total Volume	Total Volume
ID	Area (ac.)	Area (ac.)	Impervious	Runoff Coeff., R	(ac-ft)	Required (ac-ft)	Provided ^{1.} (ac-ft)
DET 110	2.31	0.93	40%	0.41	0.079	0.079	0.195

^{1.-} Volume provided below overflow weir

	(1.0 inches) x A x R
vvQv =	12
Where:	WQV = Water Quality Volume in acre-feet A = Contributing Area in acres R = 0.05 + 0.009 (1) I = Site Imperviousness as percent

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Pond No. 3 - DET 110

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 445.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	445.00	530	0.000	0.000
1.00	446.00	1,067	0.018	0.018
2.00	447.00	1,664	0.031	0.049
3.00	448.00	2,317	0.045	0.095
4.00	449.00	3,027	0.061	0.156
5.00	450.00	3,793	0.078	0.234

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 14.00	10.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 448.40	449.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	2.60	3.33	3.33
Invert El. (ft)	= 446.60	0.00	0.00	0.00	Weir Type	= 1	Broad		
Length (ft)	= 50.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 9.18	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 27.400 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	445.00	0.00				0.00	0.00			0.000		0.000
1.00	0.018	446.00	0.00				0.00	0.00			0.677		0.677
2.00	0.049	447.00	0.00				0.00	0.00			1.055		1.055
3.00	0.095	448.00	0.00				0.00	0.00			1.470		1.470
4.00	0.156	449.00	5.20 ic				5.18 s	0.00			1.920		7.103
5.00	0.234	450.00	6.44 ic				6.42 s	26.00			2.406		34.83



Appendix F Hydrologic Analysis – Existing Conditions

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023



	Curve Number Ca	alcula	ation	S		
Project: Location:	Camp Yankee Trails Site Improvements 343 Plains Road	_				
_	Tolland, Connecticut				5.4	
By:	MCB Date: 10/30/23 Cr	necked:		2 10	Date:	
Circle one.	<u>Fresent</u> Developed wat	ersneu.	EAVIC	5-10		
Soil Name and	Cover Description	CI	N Value	e ^{1.}	Area	Product
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	CN x Area
B Soil	Woods - Good Condition	55			38.17	2099.58
B Soil	Open Space - Good Condition	61			3.92	239.19
B Soil	Gravel	85			1.62	137.56
C Soil	Woods - Good Condition	70			1.70	118.66
N/A	Paved/Impervious	98			0.11	11.22
N/A	Building	98			0.63	61.97
N/A	Water	98			0.47	45.99
			Tota	als = (46.63 0.07285	2714.18 sq mi)
CN (\	weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{271}{46}$	14.18 6.63	Use	e CN =	58.2]



	Curve Number Ca	alcula	ation	S								
Project:	Camp Yankee Trails Site Improvements											
Location:	343 Plains Road	-										
	Tolland, Connecticut											
By:	By: MCB Date: 10/30/23 Checked: Date: Date:											
Circle one:	Circle one: Present <u>Developed</u> Watershed: <u>PRWS-10</u>											
Soil Name	Cover Description	С	N Value	e ^{1.}	Area	Product						
and Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	of CN x Area						
B Soil	Woods - Good Condition	55			35.27	1939.63						
B Soil	Open Space - Good Condition	61			4.75	289.50						
B Soil	Gravel	85			1.43	121.86						
C Soil	Woods - Good Condition	70			1.70	118.66						
N/A	Paved/Impervious	98			0.34	33.35						
N/A	Building	98			0.60	58.86						
N/A	Water	98			0.23	22.66						
L			l Tota	als =	44.31	2584.52						
				(0.06924	sq mi)						
CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{258}{44}$	84.52 1.31	Use	e CN =	58.3							

	Curve Number Ca	alcula	ation	S		
Project:	Camp Yankee Trails Site Improvements					
Location:	343 Plains Road	-				
	Tolland, Connecticut	_				
By:	MCB Date: 10/30/23 Ch	necked:			Date:	
Circle one:	Present <u>Developed</u> Wat	ershed:	PRWS	5-11		
Soil Name	Cover Description	С	N Value	e ^{1.}	Area	Product
and Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	of CN x Area
B Soil	Woods - Good Condition	55			0.54	29.52
B Soil	Open Space - Good Condition	61			0.84	51.40
B Soil	Gravel	85			0.06	51.40
N/A	Paved/Impervious	98			0.80	5.40
N/A	Building	98			0.07	78.21
			Tota	als =	2.31	215.92
				(0.00361	sq mi)
CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{21}{2}$	5.92 .31	- Use	e CN =	93.4	









彩SlaR



彩SbaF





NOAA Atlas 14, Volume 10, Version 3 Location name: Tolland, Connecticut, USA* Latitude: 41.9274°, Longitude: -72.3121° Elevation: m/ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	based poi	nt precipi	tation free	quency es	timates v	with 90%	confider	ice interv	vals (in in	ches) ¹
Duration				Average	recurrence	e interval (y	vears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.335 (0.255-0.439)	0.402 (0.306-0.527)	0.511 (0.389-0.674)	0.602 (0.455-0.796)	0.727 (0.534-1.00)	0.821 (0.593-1.16)	0.919 (0.646-1.34)	1.03 (0.688-1.53)	1.18 (0.764-1.82)	1.30 (0.826-2.06)
10-min	0.474 (0.362-0.621)	0.569 (0.434-0.746)	0.724 (0.550-0.953)	0.853 (0.645-1.13)	1.03 (0.756-1.42)	1.16 (0.839-1.64)	1.30 (0.915-1.90)	1.46 (0.974-2.17)	1.67 (1.08-2.58)	1.85 (1.17-2.91)
15-min	0.558 (0.426-0.731)	0.669 (0.510-0.878)	0.851 (0.647-1.12)	1.00 (0.759-1.33)	1.21 (0.890-1.67)	1.37 (0.986-1.93)	1.53 (1.08-2.23)	1.71 (1.15-2.56)	1.97 (1.27-3.04)	2.18 (1.38-3.42)
30-min	0.756 (0.577-0.991)	0.908 (0.692-1.19)	1.16 (0.880-1.52)	1.36 (1.03-1.80)	1.64 (1.21-2.27)	1.86 (1.34-2.62)	2.08 (1.46-3.03)	2.33 (1.56-3.47)	2.68 (1.73-4.13)	2.96 (1.87-4.66)
60-min	0.954 (0.729-1.25)	1.15 (0.874-1.50)	1.46 (1.11-1.92)	1.72 (1.30-2.28)	2.08 (1.53-2.87)	2.35 (1.69-3.30)	2.63 (1.85-3.83)	2.94 (1.97-4.39)	3.38 (2.19-5.22)	3.74 (2.37-5.88)
2-hr	1.22 (0.934-1.59)	1.46 (1.12-1.90)	1.85 (1.42-2.43)	2.18 (1.66-2.87)	2.63 (1.94-3.62)	2.96 (2.16-4.17)	3.32 (2.36-4.86)	3.74 (2.52-5.56)	4.37 (2.83-6.71)	4.90 (3.11-7.66)
3-hr	1.40 (1.08-1.82)	1.68 (1.29-2.19)	2.14 (1.64-2.79)	2.52 (1.92-3.30)	3.04 (2.25-4.17)	3.42 (2.50-4.80)	3.84 (2.74-5.61)	4.34 (2.92-6.42)	5.10 (3.31-7.81)	5.76 (3.66-8.98)
6-hr	1.78 (1.37-2.30)	2.14 (1.65-2.77)	2.74 (2.11-3.56)	3.24 (2.47-4.22)	3.92 (2.92-5.36)	4.42 (3.24-6.19)	4.97 (3.58-7.26)	5.65 (3.81-8.31)	6.70 (4.36-10.2)	7.62 (4.86-11.8)
12-hr	2.22 (1.72-2.86)	2.71 (2.10-3.48)	3.50 (2.70-4.51)	4.15 (3.19-5.38)	5.05 (3.78-6.88)	5.71 (4.21-7.97)	6.44 (4.66-9.37)	7.34 (4.97-10.7)	8.75 (5.72-13.2)	9.98 (6.38-15.4)
24-hr	2.64 (2.06-3.38)	3.25 (2.53-4.16)	4.25 (3.29-5.44)	5.07 (3.91-6.54)	6.21 (4.67-8.41)	7.04 (5.22-9.78)	7.96 (5.78-11.5)	9.11 (6.18-13.3)	10.9 (7.15-16.4)	12.5 (8.02-19.1)
2-day	3.00 (2.34-3.80)	3.72 (2.90-4.72)	4.90 (3.82-6.24)	5.88 (4.55-7.53)	7.23 (5.47-9.75)	8.21 (6.12-11.4)	9.30 (6.80-13.5)	10.7 (7.28-15.5)	12.9 (8.48-19.3)	14.8 (9.56-22.6)
3-day	3.26 (2.56-4.12)	4.05 (3.17-5.12)	5.33 (4.16-6.77)	6.40 (4.97-8.18)	7.87 (5.97-10.6)	8.94 (6.68-12.3)	10.1 (7.43-14.6)	11.7 (7.95-16.8)	14.1 (9.28-21.0)	16.2 (10.5-24.6)
4-day	3.49 (2.74-4.41)	4.33 (3.40-5.47)	5.70 (4.46-7.22)	6.84 (5.32-8.71)	8.40 (6.38-11.3)	9.54 (7.14-13.1)	10.8 (7.94-15.5)	12.4 (8.50-17.9)	15.0 (9.90-22.3)	17.3 (11.2-26.2)
7-day	4.14 (3.27-5.20)	5.09 (4.01-6.40)	6.64 (5.21-8.37)	7.92 (6.18-10.0)	9.69 (7.38-12.9)	11.0 (8.24-15.0)	12.4 (9.13-17.7)	14.2 (9.75-20.4)	17.1 (11.3-25.3)	19.7 (12.7-29.6)
10-day	4.80 (3.79-6.01)	5.81 (4.58-7.28)	7.45 (5.86-9.37)	8.82 (6.90-11.1)	10.7 (8.16-14.2)	12.1 (9.06-16.4)	13.6 (10.0-19.3)	15.5 (10.6-22.1)	18.5 (12.2-27.2)	21.1 (13.6-31.6)
20-day	6.87 (5.45-8.55)	7.95 (6.30-9.90)	9.71 (7.67-12.1)	11.2 (8.78-14.0)	13.2 (10.1-17.3)	14.7 (11.0-19.7)	16.3 (11.9-22.6)	18.1 (12.5-25.6)	20.8 (13.9-30.4)	23.0 (15.0-34.3)
30-day	8.63 (6.86-10.7)	9.73 (7.73-12.1)	11.5 (9.14-14.4)	13.0 (10.3-16.3)	15.1 (11.5-19.6)	16.7 (12.4-22.1)	18.3 (13.2-25.0)	20.0 (13.8-28.1)	22.3 (14.9-32.5)	24.2 (15.8-35.9)
45-day	10.8 (8.63-13.4)	12.0 (9.52-14.8)	13.8 (11.0-17.1)	15.3 (12.1-19.1)	17.4 (13.3-22.5)	19.1 (14.2-25.0)	20.7 (14.9-27.9)	22.2 (15.5-31.1)	24.2 (16.2-35.1)	25.7 (16.8-37.9)
60-day	12.7 (10.1-15.6)	13.8 (11.0-17.0)	15.7 (12.5-19.4)	17.2 (13.6-21.5)	19.4 (14.8-24.9)	21.1 (15.7-27.5)	22.7 (16.3-30.4)	24.1 (16.8-33.7)	25.9 (17.4-37.4)	27.1 (17.7-39.9)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Back to Top



PDS-based depth-duration-frequency (DDF) curves Latitude: 41.9274°, Longitude: -72.3121°

NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Thu Aug 24 13:10:38 2023

Back to Top

Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

Sample	Sample Round	L (inches)	H1(Inches)	H2(Inches)	t (min)	t (hours)	K (in/hr)	K (ft/day)
	1	3	8	6.00	1	0.017	51.429	102.857
SLR-TP-1	2	3	6.00	4.40	1	0.017	55.385	110.769
	3	3	4.40	3.10	1	0.017	62.400	124.800
	4	3	3.10	1.90	1	0.017	86.400	172.800
	5	3	1.90	0.90	1	0.017	128.571	257.143
	6							
	7							
	8							
	9							
	10							
	11							
	12							
	13							
	14							
	15							
				Sample Ave	rage		76.84	153.67

Sample	Sample Round	L (inches)	H1(Inches)	H2(Inches)	t (min)	t (hours)	K (in/hr)	K (ft/day)
	1	2	8	6.90	1	0.017	17.718	35.436
SLR-TP-2	2	2	6.90	6.00	1	0.017	16.744	33.488
	3	2	6.00	5.00	1	0.017	21.818	43.636
	4	2	5.00	4.25	1	0.017	19.459	38.919
	5	2	4.25	3.50	1	0.017	23.226	46.452
	6	2	3.50	2.75	1	0.017	28.800	57.600
	7	2	2.75	2.25	1	0.017	24.000	48.000
	8	2	2.25	1.50	1	0.017	48.000	96.000
	9	2	1.50	1.00	1	0.017	48.000	96.000
	10	2	1.00	0.50	1	0.017	80.000	160.000
	11							
	12							
	13							
	14							
	15							
				Sample Ave	rage		32.78	65.55

(76.84 + 32.78) / 2 = 54.8 in/hr 54.8 in/hr * 50% = 27.4 in/hr



Appendix G Hydrologic Analysis – Proposed Conditions

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023



Hydrographs Peak Flowrate Summary (cfs) Existing vs. Proposed

Storm Event	2yr		10yr		25yr		50yr		100yr	
	Exist	Prop								
Point of Analysis A	7.7	7.5	37.0	35.7	61.7	60.8	81.4	81.0	104.6	104.2
DET 110 W.S. Elev. (ft.) Top of Berm Elev. = 450.4	-	448.4	-	448.9	-	449.2	-	449.3	-	449.4
UG 111 W.S. Elev. (ft.) Top of Stone Elev. = 445.0	-	441.5	-	443.1	-	443.7	-	444.1	-	444.8

<u>Study Area</u> A

Sweetheart Lake

Description

Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023


Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd.	Hydrograph	Inflow		Peak Outflow (cfs)							Hydrograph
NO.	type (origin)	nyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			7.650			36.97	61.72	81.44	104.55	EXWS-10/A
3	SCS Runoff			7.496			35.61	59.28	78.10	100.14	PRWS-10
4	SCS Runoff			5.736			9.463	11.77	13.44	15.29	PRWS-11
5	Reservoir	4		0.586			5.049	7.606	9.791	11.79	DET 110
6	Reservoir	5		0.000			0.037	1.785	2.858	4.269	UG 111
7	Combine	3, 6		7.496			35.65	60.75	80.96	104.16	10 + 111 / A
Pro	Proj. file: CYT-Model01.gpw									day, 11 /	17 / 2023 109

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	7.650	3	747	1.385				EXWS-10 / A	
3	SCS Runoff	7.496	3	747	1.340				PRWS-10	
4	SCS Runoff	5.736	3	726	0.457				PRWS-11	
5	Reservoir	0.586	3	741	0.007	4	448.44	0.121	DET 110	
6	Reservoir	0.000	3	n/a	0.000	5	441.52	0.000	UG 111	
7	Combine	7.496	3	747	1.340	3, 6			10 + 111 / A	
CY	T-Model01.gp			Return P	eriod: 2 Ye	ear	Friday, 11 / 17 / 2023 110			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	36.97	3	741	4.625				EXWS-10 / A	
3	SCS Runoff	35.61	3	741	4.443				PRWS-10	
4	SCS Runoff	9.463	3	726	0.778				PRWS-11	
5	Reservoir	5.049	3	732	0.133	4	448.91	0.150	DET 110	
6	Reservoir	0.037	3	741	0.000	5	443.09	0.062	UG 111	
7	Combine	35.65	3	741	4.443	3, 6			10 + 111 / A	
	[Model01 gp				Potura P	oriod: 10 Y		Eridov 11 (17/2022	
CY	T-Model01.gp			Return P	eriod: 10 Y	'ear	Friday, 11 / 17 / 2023 111			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	61.72	3	738	7.221				EXWS-10/A	
3	SCS Runoff	59.28	3	738	6.923				PRWS-10	
4	SCS Runoff	11.77	3	726	0.981				PRWS-11	
5	Reservoir	7.606	3	729	0.219	4	449.19	0.170	DET 110	
6	Reservoir	1.785	3	744	0.035	5	443.73	0.089	UG 111	
7	Combine	60.75	3	738	6.958	3, 6			10 + 111 / A	
CY	T-Model01.gp			Return P	eriod: 25 Y	′ear	Friday, 11 / 17 / 2023 112			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	81.44	3	738	9.305				EXWS-10/A	
3	SCS Runoff	78.10	3	738	8.912				PRWS-10	
4	SCS Runoff	13.44	3	726	1.129				PRWS-11	
5	Reservoir	9.791	3	729	0.285	4	449.30	0.179	DET 110	
6	Reservoir	2.858	3	738	0.075	5	444.07	0.102	UG 111	
7	Combine	80.96	3	738	8.987	3, 6			10 + 111 / A	
	[Model01 gp				Poture			Friday 11 (17/2022	
CY	T-Model01.gp			Return F	Period: 50 Y	′ear	Friday, 11 / 17 / 2023 113			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description		
1	SCS Runoff	104.55	3	738	11.764				EXWS-10/A		
3	SCS Runoff	100.14	3	738	11.258				PRWS-10		
4	SCS Runoff	15.29	3	726	1.294				PRWS-11		
5	Reservoir	11.79	3	729	0.362	4	449.38	0.185	DET 110		
6	Reservoir	4.269	3	735	0.122	5	444.77	0.121	UG 111		
7	Combine	104.16	3	738	11.379	3, 6			10 + 111 / A		
CY	CYT-Model01.gpw				Return P	eriod: 100	Year	Friday, 11 / 17 / 2023 114			

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Pond No. 3 - DET 110

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 445.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	445.00	530	0.000	0.000
1.00	446.00	1,067	0.018	0.018
2.00	447.00	1,664	0.031	0.049
3.00	448.00	2,317	0.045	0.095
4.00	449.00	3.027	0.061	0.156
5.00	450.00	3,793	0.078	0.234

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 14.00	10.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 448.40	449.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	2.60	3.33	3.33
Invert El. (ft)	= 446.60	0.00	0.00	0.00	Weir Type	= 1	Broad		
Length (ft)	= 50.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 9.18	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 27.400 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	445.00	0.00				0.00	0.00			0.000		0.000
1.00	0.018	446.00	0.00				0.00	0.00			0.677		0.677
2.00	0.049	447.00	0.00				0.00	0.00			1.055		1.055
3.00	0.095	448.00	0.00				0.00	0.00			1.470		1.470
4.00	0.156	449.00	5.20 ic				5.18 s	0.00			1.920		7.103
5.00	0.234	450.00	6.44 ic				6.42 s	26.00			2.406		34.83

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Pond No. 1 - UG 111

Pond Data

UG Chambers -Invert elev. = 442.00 ft, Rise x Span = 2.50×4.25 ft, Barrel Len = 7.12 ft, No. Barrels = 70, Slope = 0.00%, Headers = No **Encasement -**Invert elev. = 441.50 ft, Width = 4.25 ft, Height = 3.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	441.50	n/a	0.000	0.000
0.35	441.85	n/a	0.007	0.007
0.70	442.20	n/a	0.013	0.019
1.05	442.55	n/a	0.017	0.036
1.40	442.90	n/a	0.017	0.053
1.75	443.25	n/a	0.016	0.069
2.10	443.60	n/a	0.015	0.084
2.45	443.95	n/a	0.014	0.098
2.80	444.30	n/a	0.012	0.110
3.15	444.65	n/a	0.008	0.119
3.50	445.00	n/a	0.007	0.125

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 443.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 10.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 2.00	0.00	0.00	n/a	-				
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 27.400 (1	oy Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00	-	•	

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	441.50	0.00								0.000		0.000
0.35	0.007	441.85	0.00								1.565		1.565
0.70	0.019	442.20	0.00								1.786		1.786
1.05	0.036	442.55	0.00								2.007		2.007
1.40	0.053	442.90	0.00								2.229		2.229
1.75	0.069	443.25	0.26 ic								2.450		2.712
2.10	0.084	443.60	1.30 ic								2.671		3.970
2.45	0.098	443.95	2.11 oc								2.892		5.001
2.80	0.110	444.30	3.36 oc								3.114		6.469
3.15	0.119	444.65	4.05 ic								3.335		7.390
3.50	0.125	445.00	4.63 ic								3.556		8.187



Appendix H Watershed Maps

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0080.0080

November 20, 2023







wing: W:\CADDESIGN\13280.0006-DE\CAD\CYT-HYDRO01.DWG Layout Tab:PRW tted by: JSARVER On this date: Fri, 2023 November 17 - 12:04pm





Engineering Review

December 13, 2023

Inland Wetlands & Watercourses Commission Town of Tolland c/o Michael D'Amato, Interim Wetlands Agent 21 Tolland Green Tolland, CT 06084 Via email

RE: 343 Plains Road, Camp Yankee Trails Site Improvements IWC 23-6 Engineering Review

Commission Members:

As requested, CHA reviewed the following materials for stormwater and general engineering standards that may impact the regulated area:

- Item 1Thirty (30) sheet plan set entitled "Camp Yankee Trails Site Improvements,
343 Plains Road, Tolland, Connecticut, Regulatory Drawings", prepared for Girl
Scouts of America, prepared by SLR, dated November 21, 2023Item 2Drainage Report, Camp Yankee Trails Site Improvements, 343 Plains Road,
Tolland, Connecticut, prepared by SLR, dated November 20, 2023Item 3Project Narrative, Camp Yankee Trails Site Improvements, prepared by SLR
- Item 4 Wetland Delineation Report, Camp Yankee Trails, prepared by SLR, dated January 27, 2023

CHA offers the following comments based on the Tolland LID and Stormwater Management Design Manual, 2004 Connecticut Stormwater Quality Manual, and general engineering practice:

1. CHA recommends the Designer provide rational for meeting the State or Tolland stormwater standards. The Drainage Report appears to only discuss water quality and quantity treatment.

- 2. It appears infiltration tests were performed for the stormwater basins; however, no information other than the infiltration testing rates is provided. A narrative, type of test performed, and testing locations must be provided.
- 3. Test pits are required for properly siting and designing the stormwater basins. This will provide required design information on soil types, depth to ledge and depth to groundwater. Test pit locations and logs must be provided. Based on soil mapping it appears the proposed stormwater basins are located within a type B soil; however, the very high infiltration rates obtained by the infiltration testing are not typical of a type B soil. Test pits must be provided to validate and determine the soil types.
- 4. Design and siting rational must be provided for Stormwater Basins 110 and 111 based on test pits. See Comment No. 3. Design pursuant the Tolland LID Manual or the Connecticut Stormwater Quality Manual must be provided and fully described. Calculations and descriptions such as drawdown time, depth to high groundwater, pretreatment, etc. must be provided.
- 5. Pretreatment is required for Stormwater Basin 110. CHA recommends a forebay within Stormwater Basin 110.
- 6. Although the infiltration testing supports an infiltration rate of 27.4 inches per hour, the rate will be limited by the surface soil. It does not appear that a cross section of the basin or a call out for the type of soil that will line the basin is provided. CHA recommends an engineered soil consisting of sand, loam, and compost. Typically this engineered soil provides an infiltration rate of 2.41 inches per hour. This rate would then be used as the infiltration rate in the drainage calculations for Stormwater Basin 110.
- 7. Drainage calculations for Stormwater Basin 110 use a weir elevation of 448.4. The elevation called for on the plans is 449.4. The calculations, results, and associated narrative must be revised accordingly.
- 8. The provided water quality volume based on the drainage calculations appears to be 0.156 acrefeet. The water quality chart on page 35 of the PDF indicates 0.195 acre-feet. This chart must be updated or an explanation of how the provided water quality volume was achieved must be provided.
- 9. No calculations or cross sections are provided for the "vegetated swale" on the eastern side of the proposed access road to the waterfront improvements. It is unclear if the proposed swale can properly convey runoff to the stormwater basins without impacting the waterfront area or Sweetheart Lake.
- 10. Proposed riprap is called out as both 1.5:1 and 1:1 slopes on the plan set. This call out must be consistent within the plan set.
- 11. Inspection ports for Stormwater Basin 111 must be labeled on the plan set.
- 12. Information must be provided for the beach sand construction at the waterfront improvement area. It is unclear how this area will be modified and how this may impact Sweetheart Lake.



- 13. CHA recommends sediment barrier be installed at the toe of slope (around the bottom) of Stormwater Basin 110 to prevent fines from reducing the infiltration capacity of the basin while the side slopes are being stabilized.
- 14. A sequencing plan must be provided for the construction and associated sediment and erosion control of the stormwater basins. The basins cannot be used as temporary sediment basins due to the reduction of infiltration from eroded construction fines. CHA recommends the use of a separately located temporary sediment trap to allow the construction of the stormwater basins once the upgradient site is fully stabilized.
- 15. A long-term stormwater operation and maintenance plan must be provided to ensure the stormwater management systems continue to function as designed. The location of the systems upgradient and adjacent to Sweetheart Lake make the implementation of this plan important to prevent stormwater system failures that will directly impact the Lake.
- 16. The Preformed Scour Hole Detail on Sheet SD-5 must be updated to correctly identify FES 5.

Please contact me if you have any questions regarding these comments.

Sincerely,

Chuck Eaton, P.E., LEEP-AP Tolland Town Engineer v:\projects\ehct105\projects\muni_ct\tolland\2019400.000_tolland_generalservices\application reviews\343 plains road\2023-12-13 engineering review - 343 plains rd docx





December 20, 2023

Mr. Chuck Eaton, PE, LEEP-AP CHA 400 Capital Boulevard, Suite 301 Rocky Hill, CT 06067

SLR Project No.: 141.13280.00006

RE: Response to IWC 23-6 Review Comments 343 Plains Road - Camp Yankee Trails Site Improvements Tolland, Connecticut

Dear Mr. Eaton,

SLR International Corporation (SLR) is in receipt of CHA's review comments dated December 13, 2023, regarding the above-referenced project. We offer the following responses to the comments contained therein:

General Comments

- C1. CHA recommends the designer provide rational for meeting the State or Tolland stormwater standards. The Drainage Report appears to only discuss water quality and quantity treatment.
- R1. As referenced in the Drainage Report, the design meets the requirements of the 2004 Connecticut Stormwater Quality Manual for no increases in peak flow rates for the 2-, 10-, 25-, 50-, and 100-year storms as well as the groundwater recharge volume (GRV) and water quality volume (WQV) requirements. Additionally, runoff volume control is provided in accordance with the Town of Tolland Low Impact Development manual due to the infiltrative capacity of both the stormwater basin and the underground chamber system.
- C2. It appears infiltration tests were performed for the stormwater basins; however, no information other than the infiltration testing rates is provided. A narrative, type of test performed, and testing locations must be provided.
- R2. Test pit locations are depicted on the plan set. Falling head permeability tests conforming with American Society for Testing and Materials D5084-03 were performed in SLR's in-house laboratory for two undisturbed tube samples taken at depths of 42" and 36" respectively. Results of the permeability tests are provided in Appendix F of the Drainage Report, and 50 percent of the average rate was used for design of Stormwater Basin 110 and Underground Detention System 111.
- C3. Test pits are required for properly siting and designing the stormwater basins. This will provide required design information on soil types, depth to ledge and depth to groundwater. Test pit locations and logs must be provided. Based on soil mapping it appears the proposed stormwater basins are located within a type B soil; however, the very high infiltration rates obtained by the infiltration testing are not typical of a type B soil. Test pits must be provided to validate and determine the soil types.

R3. Test pit data is included on Sheet UT-2 of the plan set.

- C4. Design and siting rational must be provided for Stormwater Basins 110 and 111 based on test pits. See comment No.3. Design pursuant the Tolland LID Manual or the Connecticut Stormwater Quality Manual must be provided and fully described. Calculations and descriptions such as drawdown time, depth to high groundwater, pretreatment, etc. must be provided.
- R4. Test pit locations are depicted on the plan set and are located between the locations of Stormwater Basin 110 and Underground Detention System 111. Drawdown time calculations have been provided in Appendix E of the Drainage Report. No groundwater was located in either test pit but can be inferred based on the water level in Sweetheart Lake, around Elevation 438.0. Pretreatment has been provided in the form of a sediment forebay in Stormwater Basin 110.
- C5. Pretreatment is required for Stormwater Basin 110. CHA recommends a forebay within Stormwater Basin 110.

R5. A sediment forebay has been added to Stormwater Basin 110.

- C6. Although the infiltration testing supports an infiltration rate of 27.4 inches per hour, the rate will be limited by the surface soil. It does not appear that a cross section of the basin or a call out for the type of soil that will line the basin is provided. CHA recommends an engineered soil consisting of sand, loam, and compost. Typically, this engineered soil provides an infiltration rate of 2.41 inches per hour. This rate would then be used as the infiltration rate in the drainage calculations for Stormwater Basin 110.
- R6. A stone wick has been added to Stormwater Basin 110, which will be hydraulically connected to an infiltration stone layer beneath the topsoil layer of the basin. This stone layer will be the same area as the bottom of the basin and will interface with the native soil, supporting the use of an infiltration rate of 27.4 inches per hour. A detail has been provided on Sheet SD-5. Onsite sandy loam soils will be used for the topsoil growing medium.
- C7. Drainage calculations for Stormwater Basin 110 use a weir elevation of 448.4. The elevation called for on the plans is 449.4. The calculations, results and associated narrative must be revised accordingly.

R7. The overflow weir elevation for Stormwater Basin 110 has been adjusted to 448.0. The callout on Sheet UT-2 has been adjusted to reflect this.

C8. The provided water quality volume based on the drainage calculations appears to be 0.156 acre-feet. The water quality chart on page 35 of the PDF indicates 0.195 acre-feet. This chart must be updated or an explanation of how the provided water quality volume was achieved must be provided.

R8. The required water quality volume is 0.079 acre-feet (ac-ft). The Drainage Report has been updated to show that the provided water quality volume is 0.177 ac-ft.

- C9. No calculations or cross sections are provided for the "vegetated swale" on the eastern side of the proposed access road to the waterfront improvements. It is unclear if the proposed swale can properly convey runoff to the stormwater basins without impacting the waterfront area or Sweetheart Lake.
- R9. Calculations for the vegetated swale have been provided in Appendix D of the Drainage Report.

- C10. Proposed riprap is called out as both 1.5:1 and 1:1 slope on the plan set. This call out must be consistent within the plan set.
- R10. The callouts on the plan set have been updated to reflect all 1.5:1 riprap slopes.
- C11. Inspection ports for Stormwater Basin 111 must be labeled on the plan set.
- R11. A callout for the inspection ports for Underground Detention System 111 has been added to Sheet UT-2.
- C12. Information must be provided for the beach sand construction at the waterfront improvement area. It is unclear how this area will be modified and how this may impact Sweetheart Lake.
- R12. A graphic cross section has been added to sheet GR-4 to illustrate the proposed work. Essentially, the waterfront area is being cut down in grade to allow for a more conducive gathering area for waterfront programming. A less steep waterfront allows for easier grouping of swimmers for instruction, provides a more relaxing area for seating and sunbathing, and reduces the erosive force of surface runoff. The waterfront area will be constructed with reused existing sand and gravel from the site. Large stones will be removed, and the material will be compacted to form the sloped waterfront access area.
- C13. CHA recommends sediment barrier be installed at the tow of slope (around the bottom) of Stormwater Basin 110 to prevent fines from reducing the infiltration capacity of the basin while the side slopes are being stabilized.
- R13. Silt fence and hay bales were added at the toe of the slope around the bottom of Stormwater Basin 110. These protections will remain in place until satisfactory vegetative cover is established on all side slopes. See Sheet SE-2.
- C14. A sequencing plan must be provided for the construction and associated sediment and erosion control of the stormwater basins. The basins cannot be used as temporary sediment basins due to the reduction of infiltration from eroded construction fines. CHA recommends the use of a separately located temporary sediment trap to allow the construction of the stormwater basins once the upgradient site is fully stabilized.
- R14. A construction sequence has been provided on Sheet SE-2. As discussed with the Inland Wetlands & Watercourse Commission, a temporary sediment trap has been added to the plans and will be located at Stormwater Basin 110. The bottom of the trap will be a foot higher than the bottom of Stormwater Basin 110. Sediment will be removed from the trap prior to basin construction.
- C15. A long-term stormwater operation and maintenance plan must be provided to ensure the stormwater management systems continue to function as designed. The location of the systems upgradient and adjacent to Sweetheart Lake make the implementation of this plan important to prevent stormwater system failures that will directly impact the lake.
- R15. A stormwater operation and maintenance plan has been included as part of the revised Drainage Report.
- C16. The Preformed Scour Hole Detail on Sheet SD-5 must be updated to correctly identify FES 5.
- R16. The preformed scour hole detail has been updated.

Please do not hesitate to contact either of the undersigned at (203) 271-1773 should you have any questions regarding this matter.

Regards,

SLR International Corporation

Michael T. Doherty, PLA US Manager of Landscape Architecture mtdoherty@slrconsulting.com

13280.00006.d1923.ltr-2.docx

Josh Pathie

Todd Ritchie, PE Principal Civil Engineer tritchie@slrconsulting.com



December 20, 2023

Mr. Michael D'Amato, Wetlands Agent Town of Tolland 21 Tolland Green, 3rd Level Tolland, CT 06084

SLR Project No.: 141.13280.00006

RE: 343 Plains Road - Camp Yankee Trails Inland Wetlands & Watercourse Commission Comments Tolland, Connecticut

Dear Mr. D'Amato,

Enclosed please find information in response to questions and concerns discussed during the December 14, 2023, Town of Tolland Inland Wetlands & Watercourse Commission regular meeting pertaining to the Girl Scouts of Connecticut permit application for proposed work at 343 Plains Road. The following discussion items were noted and are provided with a response.

- C1. Should check dams be added to the vegetated swale along the access drive to the dining hall?
- R1. The addition of check dams is not recommended due to the presence of the proposed drainage structures and the shallow depth of the proposed vegetative swale. The series of six open grate manholes, which are the full width of the swale, will provide the most efficient protection by capturing flows. Check dams are typically a minimum of 1 foot in height. At this height, the check dams will impede flow, leading water to overtop the swale and redirect runoff to adjacent areas that may be more prone to erosion.
- C2. Should the angle of the pipe exiting Manhole #6 to Stormwater Basin 110 be altered to reduce the acute angle?
- R2. The location of Manhole #6 is positioned to capture as much flow as possible before the end of the swale, which drives the angle of the pipe to the stormwater basin. The pipe conveyance computations included in the drainage report take the angle of the pipe into account for junction losses in the system. The 25-year storm is adequately conveyed by the storm drainage system.
- C3. Should additional erosion protection be provided at the turn in the swale just north of the proposed detention basin?
- R3. We do not believe additional protection is necessary due to the close proximity upgradient of Manhole #7, which should significantly reduce flows to Manhole #5 at the turn of the drive. Overall, the six 24"-diameter grate inlets at each manhole within the swale will collect water from the swale and introduce it to the pipe conveyance system. Very little water will bypass these inlets.

- C4. Should additional erosion protection be provided at the stormwater basin spillway?
- R4. The stormwater basin is designed such that water will not discharge over the spillway for up to a 100-year storm event. An additional area below the spillway has been added as shown on revised sheet UT-2.
- C5. Should additional erosion protection be provided after Manhole #6 near the bottom of the dining hall access drive?
- R5. The grading after Manhole #6 has been softened to allow for a flatter and wider area after the structure. A high point was also added after the structure to direct runoff back to the structure in moderate rain events. Any water that continues beyond the structure will be dissipated by a layer of crushed stone that has been added to further slow flows before reaching the paved access drive. It should also be noted that the proposed grades in this area are less steep than existing conditions.
- C6. Can surface runoff be slowed at the slope between the proposed accessible beach access and the existing boat house building?
- R6. A stone infiltration trench is proposed along the northern edge of the accessible ramp and sloped walkway, which will assist in diffusing and slowing upland flows. The existing topography in this area is sloped at a similar angle to the proposed and experiences limited erosion. We expect the establishment of greater vegetative cover to further limit the potential for erosive action; however, an erosion control blanket has been added to the plans for added protection until a satisfactory vegetative cover is established.

Please feel free to contact either of the undersigned should you need any further information.

Regards,

SLR International Corporation

Michael T. Doherty, PLA US Manager of Landscape Architecture mtdoherty@slrconsulting.com

13280.00006.d1923.ltr-1.docx

Josh Pathe

Todd Ritchie, PE Principal Civil Engineer tritchie@slrconsulting.com

₩SLR

Camp Yankee Trails Site Improvements

343 Plains Road Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

20 Washington Avenue North Haven, CT 06473

Prepared by:

SLR International Corporation

99 Realty Drive, Cheshire, Connecticut, 06410

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023

Making Sustainability Happen

Drainage Report

Camp Yankee Trails Site Improvements 343 Plains Road Tolland, Connecticut SLR #141.13280.000006.0060

This Drainage Report has been prepared in support of the proposed upgrades to the existing Girl Scouts camp on Plains Road in the town of Tolland, Connecticut. This project includes renovations and additions to the dining hall, a new shower house, and four new cabins including an Americans with Disabilities Act (ADA) accessible unit, a new parking lot, stone dust and concrete paths, an access road, and stormwater improvements.



Figure 1 – 343 Plains Road, Map, Block, Lot (MBL): 06-A-001

Table 1 – Stormwater Data

Parcel Size Total	221 acres
Existing Impervious Area (Watershed Area)	0.74 acres
Proposed Impervious Area (Watershed Area)	1.79 acres
Soil Type (Hydrologic Soil Group)	"B" and "C"
Existing Land Use	Open space, woods, gravel, water, building, and paved/impervious cover
Proposed Land Use	Open space, woods, gravel, water, building, and paved/impervious cover
Design Storm for Stormwater Management	No increases in peak rates of runoff for the 2-, 10-, 25-, 50-, and 100-year storms; Connecticut Department of Energy & Environmental Protection (CTDEEP) water quality volume (WQV) and groundwater recharge volume (GRV), Runoff Volume Control per Town of Tolland
Water Quality Measures	Catch basins with 2-foot sumps, underground detention system, and retention/infiltration storage for WQV
Design Storm for Storm Drainage	25-year storm
Federal Emergency Management Agency (FEMA) Special Flood Hazard Areas	Area of Minimal Flood Hazard (Zone X)
Connecticut Department of Energy & Environmental Protection Aquifer Protection Areas	None

Stormwater Management Approach

The proposed stormwater management system for the project focuses on providing water quality management while attenuating proposed peak flows. Water quality treatment in accordance with the CTDEEP requirements for WQV is provided. The proposed stormwater treatment train consists of catch basins with 2-foot sumps and retention/infiltrations storage for the WQV.

The computer program entitled *Hydraflow Storm Sewers Extension for AutoCAD*[®] *Civil 3D*[®] *2023* by Autodesk, Inc. was used for designing the proposed storm drainage collection system. Storm drainage computations performed include pipe capacity and hydraulic grade line calculations. The contributing watershed to each individual catch basin inlet was delineated to determine the drainage area and land coverage. These values were used to determine the stormwater runoff to each inlet using the Rational Method. The rainfall intensities for the site were obtained from the National Oceanic and Atmospheric Administration (NOAA) Atlas 14,

Volume 10, Precipitation Frequency Data Server (PFDS). The proposed storm drainage system is designed to provide adequate capacity to convey the 25-year storm event.

Water Quality Management

Water quality measures or Best Management Practices (BMPs) have been incorporated into the design to maintain water quality to provide protection of the areas downgradient of the proposed development. The proposed stormwater management system will include catch basins with 2-foot sumps and retention/infiltration storage for the WQV and GRV.

The proposed stormwater basin will provide retention volume along its bottom, thus creating a water quality feature within it. This serves several purposes, including stormwater renovation and first-flush retention. The vegetation will provide pollutant removal by filtering stormwater runoff and utilizing excess nutrients that may be present in the stormwater. The CTDEEP *2004 Stormwater Quality Manual* (Chapter 7) recommends methods for sizing stormwater treatment measures with WQV and GRV computations. The WQV addresses the initial stormwater runoff, also commonly referred to as the "first-flush" runoff. The WQV provides adequate volume to store the runoff associated with the first 1 inch of rainfall, which tends to contain the highest concentration of potential pollutants. Supporting calculations have been included in the Appendix of this report.

Hydrologic Analysis

A hydrologic analysis was conducted to analyze the predevelopment and postdevelopment peak-flow rates from the site. One analysis point was selected, as it receives all runoff from the site. Analysis Point A represents Sweetheart Lake. The total watershed area delineated is approximately 46.6 acres under both existing and proposed conditions.

The method of predicting the surface water runoff rates utilized in this analysis was a computer program titled *Hydraflow Hydrographs Extension for AutoCAD*[®] *Civil 3D*[®] *2019* by Autodesk, Inc., Version 2020. The *Hydrographs* program is a computer model that utilizes the methodologies set forth in the *Technical Release No. 55* (TR-55) manual and *Technical Release No. 20* (TR-20) computer model, originally developed by the United States Department of Agriculture – Natural Resources Conservation Service (USDA-NRCS). The *Hydrographs* computer modeling program is primarily used for conducting hydrology studies such as this one.

The *Hydrographs* computer program forecasts the rate of surface water runoff based upon several factors. The input data includes information on land use, hydrologic soil type, vegetation, contributing watershed area, time of concentration, rainfall data, storage volumes, and the hydraulic capacity of structures. The computer model predicts the amount of runoff as a function of time, with the ability to include the attenuation effect due to dams, lakes, large wetlands, floodplains, and stormwater management basins. The input data for rainfalls with statistical recurrence frequencies of 2, 10, 25, 50, and 100 years was obtained from the NOAA Atlas 14, Volume 10 database. The corresponding rainfall totals are listed below.

Storm Frequency	Rainfall (inches)			
2-year	3.25			
10-year	5.07			
25-year	6.21			
50-year	7.04			
100-year	7.96			

Land use for the site under existing and proposed conditions was determined from field survey and aerial photogrammetry. Land use types used in the analysis included grassed or open space, woods, water, gravel, building, and impervious (paved) cover. Soil types in the watershed were determined from the CTDEEP Geographic Information System (GIS) database of the USDA-NRCS soil survey for Tolland County, Connecticut. For the analysis, the site was determined to contain hydrologic soil types "B" and "C" as classified by USDA-NRCS. Composite runoff Curve Numbers (CN) for each subwatershed were calculated based on the different land use and soil types. The time of concentration (Tc) was estimated for each subwatershed using the TR-55 methodology and was computed by summing all travel times through the watershed as sheet flow, shallow concentrated flow, and channel flow.

The existing conditions were modeled with the *Hydrographs* program to determine the peak-flow rates for the various storm events at the analysis point. A revised model was developed incorporating the proposed site conditions, the underground chamber system, and the stormwater management basin. The flows obtained with the revised model were then compared to the results of the existing conditions model. Peak-flow rates from the project site were controlled by the storage volume provided within the stormwater management basin and the underground chamber system.

The following peak rates and volumes of runoff were obtained from the *Hydrographs* hydrology results:

Analysis Point A – Sweetheart Lake					
	Peak Runoff Rate (cubic feet per second)				
Storm Frequency (years)	2	10	25	50	100
Existing Conditions	7.7	37.0	61.7	81.4	104.6
Proposed Conditions	7.5	36.2	61.7	81.2	104.2

Analysis Point A – Sweetheart Lake					
	Peak Runoff Volume (acre-feet)				
Storm Frequency (years)	2	10	25	50	100
Existing Conditions	1.38	4.62	7.22	9.30	11.8
Proposed Conditions	1.34	4.45	6.98	9.01	11.4

Detention Basin 110*					
	Water Surface Elevation (feet)				
Storm Frequency (years)	2 10 25 50 1				
Proposed Conditions	447.6	448.2	448.6	448.9	449.1

*Top of Berm Elevation = 450.2

Underground Chamber System 111**					
	Water Surface Elevation (feet)				
Storm Frequency (years)	2	10	25	50	100
Proposed Conditions	441.5	443.4	444.1	444.3	444.8

**Top of Stone Elevation = 445.0

Conclusion

The results of the hydrologic analysis demonstrate that there will be no increases in peak-flow rates and volumes from the proposed development. This was achieved for storm events modeled through a planned stormwater management system with a subsurface infiltration system and stormwater management basin. The proposed development will also introduce a new stormwater treatment train consisting of catch basins with 2-foot sumps and retention/infiltration of the WQV and GRV.

All supporting documentation and stormwater-related computations are attached to this report along with the *Hydrographs* model results for stormwater management and *Hydraflow Storm Sewers* model results for the proposed storm drainage system. Illustrative watershed maps for both existing and proposed conditions are also attached to this report.

Appendices

- Appendix A United States Geological Survey Location Map
- Appendix B Federal Emergency Management Agency Flood Insurance Rate Map
- Appendix C Natural Resources Conservation Service Hydrologic Soil Group Map
- Appendix D Storm Drainage Computations
- Appendix E Water Quality Computations
- Appendix F Hydrologic Analysis Input Computations
- Appendix G Hydrologic Analysis Computer Model Results
- Appendix H Operations and Maintenance Manual
- Appendix I Watershed Maps

13280.00006.0080.n2023.rpt.docx



Appendix A United States Geological Survey Location Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023





Copyright SLR Consulting, Inc - 2023



Appendix B FEMA Flood Insurance Rate Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023







Appendix C Natural Resources Conservation Service Hydrologic Soil Group Map

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023





National Cooperative Soil Survey

Conservation Service

Page 1 of 4



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at

Please rely on the bar scale on each map sheet for map

Source of Map: Natural Resources Conservation Service Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut Survey Area Data: Version 22, Sep 12, 2022

Soil map units are labeled (as space allows) for map scales

Date(s) aerial images were photographed: Jun 14, 2022-Oct 6,

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	1.8	0.6%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	B/D	0.0	0.0%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	В	42.9	15.2%
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	В	8.4	3.0%
71C	Nipmuck-Brimfield-Rock outcrop complex, 3 to 15 percent slopes	В	17.4	6.2%
71E	Nipmuck-Brimfield-Rock outcrop complex, 15 to 45 percent slopes	В	47.9	17.0%
72C	Nipmuck-Brookfield complex, 3 to 15 percent slopes, very rocky	В	33.5	11.9%
72E	Nipmuck-Brookfield complex, 15 to 45 percent slopes, very rocky	В	40.5	14.4%
85C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes, very stony	С	35.3	12.5%
109	Fluvaquents-Udifluvents complex, frequently flooded	B/D	39.6	14.1%
W	Water		14.2	5.0%
Totals for Area of Inter	est	281.6	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



Appendix D Storm Drainage Computations

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023


Project:	Camp Yankee	Trails Site Imp	rovement		By:	JLS	Date:	11/16/23
Location:	343 Plains Roa	d, Tolland, CT			Checked:	MCB	Date:	11/17/23
Basin Name	Impervious Area C=0.9 (sf)	Grassed Area C=0.3 (sf)	Gravel Area C=0.6 (sf)	Wooded Area C=0.2 (sf)	Total Area (sf)	Total Area (ac)	Weighted C	Tc (min)
			Sys	stem 110				
MH 5	907	848	0	32	1787	0.04	0.60	5.0
MH 6	2207	6311	512	6753	15783	0.36	0.35	5.0
MH 7	5492	5055	0	9041	19588	0.45	0.42	5.0
MH 8	3270	3165	0	0	6435	0.15	0.60	5.0
MH 9	1793	1899	219	294	4205	0.10	0.56	5.0
MH 10	969	535	0	0	1504	0.03	0.69	5.0
CLCB 11	11775	3336	0	0	15111	0.35	0.77	5.0
CLCB 12	7651	5971	0	0	13622	0.31	0.64	5.0
YD 13	432	392	0	0	824	0.02	0.61	5.0
CLCB 14	1881	347	0	0	2228	0.05	0.81	5.0
YD 15	818	343	0	0	1161	0.03	0.72	5.0
YD 16	0	603	0	0	603	0.01	0.30	5.0

. _ _

Storm Sewer IDF Curves





NOAA Atlas 14, Volume 10, Version 3 Location name: Tolland, Connecticut, USA* Latitude: 41.9274°, Longitude: -72.3121° Elevation: 579 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	ased poir	nt precipit	ation freq	luency es	timates w	ith 90% c	onfidence	intervals	(in inches	s/hour) ¹
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	4.02 (3.06-5.27)	4.82 (3.67-6.32)	6.13 (4.67-8.09)	7.22 (5.46-9.55)	8.72 (6.41-12.0)	9.85 (7.12-13.9)	11.0 (7.75-16.1)	12.3 (8.26-18.4)	14.2 (9.17-21.9)	15.7 (9.91-24.7)
10-min	2.84 (2.17-3.73)	3.41 (2.60-4.48)	4.34 (3.30-5.72)	5.12 (3.87-6.77)	6.18 (4.54-8.52)	6.98 (5.03-9.82)	7.81 (5.49-11.4)	8.73 (5.84-13.0)	10.0 (6.49-15.5)	11.1 (7.02-17.5)
15-min	2.23 (1.70-2.92)	2.68 (2.04-3.51)	3.40 (2.59-4.48)	4.01 (3.04-5.30)	4.84 (3.56-6.68)	5.47 (3.94-7.70)	6.13 (4.30-8.93)	6.85 (4.59-10.2)	7.87 (5.09-12.2)	8.70 (5.51-13.7)
30-min	1.51 (1.15-1.98)	1.82 (1.38-2.38)	2.31 (1.76-3.04)	2.72 (2.06-3.60)	3.29 (2.42-4.54)	3.72 (2.68-5.23)	4.16 (2.92-6.07)	4.65 (3.12-6.94)	5.35 (3.46-8.26)	5.91 (3.74-9.31)
60-min	0.954 (0.729-1.25)	1.15 (0.874-1.50)	1.46 (1.11-1.92)	1.72 (1.30-2.28)	2.08 (1.53-2.87)	2.35 (1.69-3.30)	2.63 (1.85-3.83)	2.94 (1.97-4.39)	3.38 (2.19-5.22)	3.74 (2.37-5.88)
2-hr	0.609	0.730	0.927	1.09	1.32	1.48	1.66	1.87	2.18	2.45
	(0.467-0.794)	(0.559-0.952)	(0.707-1.21)	(0.828-1.43)	(0.972-1.81)	(1.08-2.09)	(1.18-2.43)	(1.26-2.78)	(1.42-3.36)	(1.55-3.83)
3-hr	0.467	0.559	0.711	0.837	1.01	1.14	1.28	1.44	1.70	1.92
	(0.358-0.606)	(0.429-0.727)	(0.544-0.927)	(0.637-1.10)	(0.749-1.39)	(0.831-1.60)	(0.912-1.87)	(0.971-2.14)	(1.10-2.60)	(1.22-2.99)
6-hr	0.296 (0.229-0.383)	0.358 (0.276-0.462)	0.457 (0.351-0.593)	0.540 (0.413-0.704)	0.654 (0.488-0.895)	0.738 (0.541-1.03)	0.829 (0.597-1.21)	0.943 (0.636-1.39)	1.12 (0.728-1.70)	1.27 (0.811-1.97)
12-hr	0.184	0.224	0.290	0.344	0.419	0.474	0.534	0.609	0.726	0.828
	(0.143-0.236)	(0.173-0.288)	(0.223-0.374)	(0.264-0.446)	(0.314-0.570)	(0.349-0.661)	(0.386-0.777)	(0.412-0.891)	(0.474-1.10)	(0.529-1.28)
24-hr	0.110	0.135	0.177	0.211	0.258	0.293	0.331	0.379	0.454	0.520
	(0.085-0.140)	(0.105-0.173)	(0.137-0.226)	(0.163-0.272)	(0.194-0.350)	(0.217-0.407)	(0.241-0.480)	(0.257-0.552)	(0.298-0.683)	(0.334-0.797)
2-day	0.062	0.077	0.102	0.122	0.150	0.171	0.193	0.222	0.268	0.309
	(0.048-0.079)	(0.060-0.098)	(0.079-0.130)	(0.094-0.156)	(0.113-0.203)	(0.127-0.236)	(0.141-0.280)	(0.151-0.322)	(0.176-0.401)	(0.199-0.470)
3-day	0.045	0.056	0.074	0.088	0.109	0.124	0.140	0.161	0.195	0.225
	(0.035-0.057)	(0.044-0.071)	(0.057-0.094)	(0.069-0.113)	(0.082-0.147)	(0.092-0.171)	(0.103-0.202)	(0.110-0.233)	(0.128-0.291)	(0.145-0.341)
4-day	0.036	0.045	0.059	0.071	0.087	0.099	0.112	0.129	0.156	0.180
	(0.028-0.045)	(0.035-0.056)	(0.046-0.075)	(0.055-0.090)	(0.066-0.117)	(0.074-0.136)	(0.082-0.161)	(0.088-0.186)	(0.103-0.232)	(0.116-0.272)
7-day	0.024	0.030	0.039	0.047	0.057	0.065	0.073	0.084	0.101	0.117
	(0.019-0.030)	(0.023-0.038)	(0.031-0.049)	(0.036-0.059)	(0.043-0.076)	(0.049-0.089)	(0.054-0.105)	(0.058-0.121)	(0.067-0.150)	(0.075-0.176)
10-day	0.019	0.024	0.031	0.036	0.044	0.050	0.056	0.064	0.076	0.087
	(0.015-0.025)	(0.019-0.030)	(0.024-0.039)	(0.028-0.046)	(0.034-0.059)	(0.037-0.068)	(0.041-0.080)	(0.044-0.092)	(0.050-0.113)	(0.056-0.131)
20-day	0.014	0.016	0.020	0.023	0.027	0.030	0.033	0.037	0.043	0.048
	(0.011-0.017)	(0.013-0.020)	(0.015-0.025)	(0.018-0.029)	(0.020-0.035)	(0.022-0.040)	(0.024-0.047)	(0.026-0.053)	(0.028-0.063)	(0.031-0.071)
30-day	0.011	0.013	0.016	0.018	0.020	0.023	0.025	0.027	0.030	0.033
	(0.009-0.014)	(0.010-0.016)	(0.012-0.019)	(0.014-0.022)	(0.015-0.027)	(0.017-0.030)	(0.018-0.034)	(0.019-0.038)	(0.020-0.045)	(0.021-0.049)
45-day	0.010	0.011	0.012	0.014	0.016	0.017	0.019	0.020	0.022	0.023
	(0.007-0.012)	(0.008-0.013)	(0.010-0.015)	(0.011-0.017)	(0.012-0.020)	(0.013-0.023)	(0.013-0.025)	(0.014-0.028)	(0.015-0.032)	(0.015-0.035)
60-day	0.008	0.009	0.010	0.011	0.013	0.014	0.015	0.016	0.017	0.018
	(0.007-0.010)	(0.007-0.011)	(0.008-0.013)	(0.009-0.014)	(0.010-0.017)	(0.010-0.019)	(0.011-0.021)	(0.011-0.023)	(0.012-0.025)	(0.012-0.027)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top









NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Thu Aug 24 13:11:05 2023

Back to Top

Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Project File: System 110.stm	Number of lines: 12	Date: 11/17/2023
------------------------------	---------------------	------------------

Storm Sewer Inventory Report

Line		Align	ment			Flow	Data					Physical	Data				Line ID
NO.	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	61	-13	Grate	0.00	0.36	0.35	5.0	445.00	4 10	447 50	12	Cir	0.012	1 50	452 50	OUTEAU - MH 6
2	1	78	-103	Grate	0.00	0.04	0.60	5.0	449.20	10.00	457.00	12	Cir	0.012	1.00	461.00	MH 6 - MH 5
3	2	47	52	Grate	0.00	0.45	0.42	5.0	458.20	10.00	462.90	12	Cir	0.012	0.51	469.50	MH 5 - MH 7
4	3	99	17	Grate	0.00	0.15	0.60	5.0	466.50	8.28	474 70	12	Cir	0.012	0.92	477 70	MH 7 - MH 8
5	4	133	-34	Grate	0.00	0.10	0.56	5.0	474.70	6.62	483.50	12	Cir	0.012	0.81	488.50	MH 8 - MH 9
6	5	78	-29	Grate	0.00	0.03	0.69	5.0	485.50	9.87	493.20	12	Cir	0.012	1.33	499.44	MH 9 - MH 10
7	6	59	-2	Grate	0.00	0.05	0.81	5.0	495.50	10.17	501.50	12	Cir	0.012	1.32	505.00	MH 10 - CLCB 14
8	7	34	-59	DrGrt	0.00	0.03	0.72	5.0	502.00	3.53	503.20	12	Cir	0.012	1.37	506.20	CLCB 14 - YD 15
9	8	66	63	DrGrt	0.00	0.01	0.30	5.0	503.70	3.18	505.80	8	Cir	0.012	1.00	508.30	YD 15 - YD 16
10	6	41	-60	Grate	0.00	0.35	0.77	5.0	495.50	9.76	499.50	12	Cir	0.012	0.81	504.00	MH 10 - CLCB 11
11	10	122	-29	Grate	0.00	0.31	0.64	5.0	501.00	1.64	503.00	12	Cir	0.012	1.50	506.00	CLCB 11 - CLCB 12
12	11	47	94	DrGrt	0.00	0.02	0.61	5.0	503.00	2.13	504.00	12	Cir	0.012	1.00	507.00	CLCB 12 - YD 13
Project I	I File: Syste	em 110.stm	ו ו	I	<u> </u>	1	I	I	<u> </u>	1	<u> </u>	Number o	f lines: 12	1	<u> </u>	Date: 1	1/17/2023

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	с	Тс		Rain	Total	Сар	Vel	Pipe		Invert El	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
Line	То		Incr	Total	coen	Incr	Total	Inlet	Syst	0	now	Tuli		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	61	0.36	1.90	0.35	0.13	1.05	5.0	7.1	7.4	7.80	7.81	9.94	12	4.10	445.00	447.50	449.10	451.60	447.36	452.50	OUTFALL - MH 6
2	1	78	0.04	1.54	0.60	0.02	0.92	5.0	7.0	7.5	6.93	12.20	8.86	12	10.00	449.20	457.00	453.90	457.97	452.50	461.00	MH 6 - MH 5
3	2	47	0.45	1.50	0.42	0.19	0.90	5.0	6.9	7.5	6.78	12.20	12.33	12	10.00	458.20	462.90	458.73	463.87	461.00	469.50	MH 5 - MH 7
4	3	99	0.15	1.05	0.60	0.09	0.71	5.0	6.8	7.6	5.42	11.10	10.57	12	8.28	466.50	474.70	466.99	475.64	469.50	477.70	MH 7 - MH 8
5	4	133	0.10	0.90	0.56	0.06	0.62	5.0	6.4	7.8	4.85	9.92	6.41	12	6.62	474.70	483.50	475.64	484.41	477.70	488.50	MH 8 - MH 9
6	5	78	0.03	0.80	0.69	0.02	0.57	5.0	6.3	7.9	4.45	12.12	10.16	12	9.87	485.50	493.20	485.92	494.08	488.50	499.44	MH 9 - MH 10
7	6	59	0.05	0.09	0.81	0.04	0.07	5.0	5.8	8.1	0.53	12.30	5.22	12	10.17	495.50	501.50	495.64	501.80	499.44	505.00	MH 10 - CLCB 14
8	7	34	0.03	0.04	0.72	0.02	0.02	5.0	5.6	8.3	0.20	7.25	3.04	12	3.53	502.00	503.20	502.12	503.38	505.00	506.20	CLCB 14 - YD 15
9	8	66	0.01	0.01	0.30	0.00	0.00	5.0	5.0	8.7	0.03	2.33	1.74	8	3.18	503.70	505.80	503.75	505.87	506.20	508.30	YD 15 - YD 16
10	6	41	0.35	0.68	0.77	0.27	0.48	5.0	6.2	7.9	3.80	12.05	9.52	12	9.76	495.50	499.50	495.89	500.33	499.44	504.00	MH 10 - CLCB 11
11	10	122	0.31	0.33	0.64	0.20	0.21	5.0	5.8	8.2	1.72	4.94	4.77	12	1.64	501.00	503.00	501.41	503.56	504.00	506.00	CLCB 11 - CLCB
12	11	47	0.02	0.02	0.61	0.01	0.01	5.0	5.0	8.7	0.11	5.63	0.97	12	2.13	503.00	504.00	503.56	504.13	506.00	507.00	CLCB 12 - YD 13
Proje	ct File:	System	n 110.stn	n												Number	of lines: 1	2		Run Da	te: 11/17/2	2023
	ES:Inte	nsity = 4	1.75 / (I	nlet time	+ 3.80)	^ 0.72; I	Return p	eriod =Y	′rs. 25;	c = cir	e = ellip	b = box										

Hydraulic Grade Line Computations

Lin	e Size	Q			D	ownstre	eam				Len				Upstr	eam				Chec	k	JL	Minor
	(i.e.)	(Invert elev	HGL elev	Depth	Area	Vel	Vel head	EGL elev	Sf	(54)	Invert elev	HGL elev	Depth	Area	Vel	Vel head	EGL elev	Sf	Ave Sf	Enrgy loss	coen	1055
	(in)		(π)	(π)	(ft)	(sqit)	(105)	(ft)	(π)	(%)	(ft)	(π)	(ft)	(ft)	(sqit)	(105)	(ft)	(π)	(%)	(%)	(ft)	(n)	(ft)
1	12	7.80	445.00	449.10	1.00	0.79	9.94	1.54	450.64	4.093	61	447.50	451.60	1.00	0.79	9.94	1.53	453.13	4.091	4.092	2.496	1.50	2.30
2	12	6.93	449.20	453.90	1.00	0.78	8.83	1.21	455.11	3.232	78	457.00	457.97 j	0.97**	0.78	8.89	1.23	459.20	2.861	3.047	n/a	1.23	n/a
3	12	6.78	458.20	458.73	0.53*	0.43	15.94	1.18	459.91	0.000	47	462.90	463.87	0.97**	0.78	8.71	1.18	465.05	0.000	0.000	n/a	0.51	0.60
4	12	5.42	466.50	466.99	0.49*	0.39	14.04	0.78	467.77	0.000	99	474.70	475.64	0.94**	0.76	7.09	0.78	476.42	0.000	0.000	n/a	0.92	n/a
5	12	4.85	474.70	475.64	0.94	0.75	6.34	0.65	476.29	0.000	133	483.50	484.41 j	0.91**	0.75	6.47	0.65	485.06	0.000	0.000	n/a	0.81	0.53
6	12	4.45	485.50	485.92	0.42*	0.31	14.24	0.57	486.49	0.000	78	493.20	494.08	0.88**	0.73	6.07	0.57	494.65	0.000	0.000	n/a	1.33	0.76
7	12	0.53	495.50	495.64	0.14*	0.07	7.80	0.11	495.75	0.000	59	501.50	501.80	0.30**	0.20	2.65	0.11	501.91	0.000	0.000	n/a	1.32	n/a
8	12	0.20	502.00	502.12	0.12*	0.05	4.04	0.06	502.18	0.000	34	503.20	503.38	0.18**	0.10	2.04	0.06	503.45	0.000	0.000	n/a	1.37	0.09
9	8	0.03	503.70	503.75	0.05*	0.01	2.22	0.02	503.77	0.000	66	505.80	505.87	0.07**	0.02	1.26	0.02	505.90	0.000	0.000	n/a	1.00	0.02
10) 12	3.80	495.50	495.89	0.39*	0.28	13.59	0.46	496.35	0.000	41	499.50	500.33	0.83**	0.70	5.46	0.46	500.79	0.000	0.000	n/a	0.81	0.38
1	12	1.72	501.00	501.41	0.41*	0.30	5.72	0.23	501.63	0.000	122	503.00	503.56	0.56**	0.45	3.82	0.23	503.78	0.000	0.000	n/a	1.50	0.34
12	2 12	0.11	503.00	503.56	0.56	0.06	0.24	0.05	503.60	0.000	47	504.00	504.13 j	0.13**	0.06	1.71	0.05	504.18	0.000	0.000	n/a	1.00	0.05
P	oject File:	System 1	10.stm	1	1	1	<u> </u>	1	1	1	1		1	 N	umber o	f lines: 1	2	<u> </u>	Rur	n Date:	11/17/20	1 23	<u> </u>
	ntes: * den	th assum	ed: ** Criti	cal denth ·	i-l ine co	ntaine b	vd iumn	= .	ir e = ellin	h = hor									[
''	5.00. dop	an abbann		cai dopini.,	, <u></u>	incumo n	ja. jamp	,	o omp	2 204													

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Inventory Report

Line		Align	ment			Flow	Data					Physical	Data				Line ID		
NO.	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)			
1	End	49.000	-76.000	None	11.80	0.00	0.00	0.0	442.00	9.39	446.60	12	Cir	0.012	1.00	449.00	MH 3 - OCS 110		
2	End	40.000	-109.000	мн	4.27	0.00	0.00	0.0	441.00	5.00	443.00	12	Cir	0.012	1.00	446.40	OUTFALL - MH 2		
Project	File: Syste	em 120.stm	ו							Number of lines: 2 Date: 11/17/2023									

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс		Rain	Total	Cap	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Ri	im Elev	Line ID
Line	To		Incr	Total	coen	Incr	Total	Inlet	Syst		now	lun		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	49 000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	11 80	11 82	15.03	12	9.39	442 00	446 60	449.30	453 89	447 00	449.00	MH 3 - OCS 110
2	End	40.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	4 27	8.63	5.66	12	5.00	441.00	443.00	442.00	443.87	442 10	446 40	OUTFALL - MH 2
	Lind	10.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	1.27	0.00	0.00		0.00		110.00	112.00	110.07	112.10		
Proje	ct File:	System	n 120.str	n												Number	of lines: 2	2		Run Da	te: 11/17/2	2023
	ES:Inte	nsity = 5	52.80 / (I	nlet time	e + 3.80)	^ 0.72;	Return p	eriod =Y	′rs. 100	; c = cir	e = ellip	b = ba	х									

Hydraulic Grade Line Computations

Line	Size	Q			D	ownstre	am				Len				Upstr	eam				Chec	k	JL	Minor
	(in)	(cfs)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sɑft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	(ft)	Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sɑft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy Ioss (ft)	(K)	(ft)
1	12	11.80	442.00	449.30	1.00	0.79	15.03	3.51	452.81	9.359	49.000	446.60	453.89	1.00**	0.79	15.02	3.51	457.40	9.355	9.357	4.585	1.00	3.51
2	12	4.27	441.00	442.00	1.00*	0.72	5.44	0.46	442.46	1.225	40.000	443.00	443.87 j	0.87**	0.72	5.89	0.54	444.41	1.119	1.172	n/a	1.00	n/a
Pro	oject File: S	System 1	20.stm											N	umber o	f lines: 2			Rur	n Date: 1	11/17/20	23	
No	tes: * dept	h assum	ed; ** Critio	cal depth.;	j-Line co	ontains h	yd. jump	; c = ci	ir e = ellip	b = box													

Storm Sewers v2023.00

Page 1

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Vegetated Swale

Trapezoidal

Tupozolau	
Bottom Width (ft)	= 2.00
Side Slopes (z:1)	= 1.50, 1.50
Total Depth (ft)	= 0.50
Invert Elev (ft)	= 475.00
Slope (%)	= 16.70
N-Value	= 0.024

Calculations

Compute by: No. Increments Q vs Depth

= 10

Highlighted

Depth (ft)	=	0.50
Q (cfs)	=	17.65
Area (sqft)	=	1.38
Velocity (ft/s)	=	12.84
Wetted Perim (ft)	=	3.80
Crit Depth, Yc (ft)	=	0.50
Top Width (ft)	=	3.50
EGL (ft)	=	3.06

Total 25-Year Storm Flow to Basin is 7.48 cfs << 17.65 cfs



Tuesday, Dec 19 2023

Outlet Protection	Calculations
--------------------------	--------------

-

<u>Project:</u> <u>Location:</u> <u>Outlet I.D.</u>	Camp Yankee Trails S 343 Plains Road, Tolla <u>FES 1</u>	Site Im and, Co	provement onnecticut	<u>By:</u> JLS <u>Checked:</u> MCB	<u>Date:</u> <u>Date:</u>	11/17/23 11/17/23			
*Based on Connecticut DOT Drainage Manual, Section 11.13									
Description FES 1	<u>n:</u>								
<u>Design Cri</u>	teria (100-yr Storm Eve	ent):							
Q (cfs)	= 4.27	$R_p(ft) =$	1						
D (in) =	12 8	$S_p(ft) =$	1						
V (fps)	= 5.66 1	⁻w (ft)=	1						
Q= Flov	<i>w</i> rate at discharge point	t in cub	ic feet per second	t (cfs)					
D= Out	let pipe diameter (in)			. (0.0)					
V= Flov	v velocity at discharge p	oint (ft/	′s)						
R _p = Ma	ximum inside pipe rise ((ft)							
S _p = insi T	ide diametere for circula	r sectio	ons of maximum i	nside pipe span for non	-circular	sections (ft)			
I _w = ⊺ai	liwater depth (ft)								
Based on	Table 11-13 1 us		> 'B'> TW/> ∩ 5	Rn					
Dasca on		ве турс	, D 1W2 0.3						
Rip Rap St	one Size:								
Velocity	<u>/</u> Rip Rap Specifi	<u>cation</u>		D ₅₀ Stone Size					
0-8 fp	s Modified			5 inches					
Durformerd									
F(ft)=0	5(R)	<u>ns:</u> =	n/a						
C(ft)=3.	.0(S _n)+6.0(F)	=	n/a						
B(ft)=2.	$0(S_p)+6.0(F)$	=	n/a						
<u>Rip Rap Sp</u>	blash Pad Dimensions	<u>.</u>							
L _a		=	10	ft					
VV1 = 3	$U(S_p)$ min.	=	3	π					
W2 = 3	.0(Sp)+0.4(La) min.	-	(Π					
d (Dept	n or Stone)	-	12	inches					



Outlet Protection Calculations										
Project:Camp Yankee Trails Site ImprovementBy:JLSDate:11/17/2023Location:343 Plains Road, Tolland, ConnecticutChecked:MCBDate:11/17/2023Outlet I.D.FES 5										
*Based on C	Connecticut DOT Dr	ainage Manual, Section 11.	<u>13</u>							
Description FES 5	Description: FES 5									
Design Crit	eria (25-yr Storm E	<u>event):</u>								
Q (cfs) =	= 7.8	$R_{p}(ft)=$	1							
D (in) =	12	$S_{p}(ft) =$	1							
V (fps) =	= 9.94	Tw (ft)=	4.1							
V= Flow R _p = Max S _p = insid T _w = Tail <u>Based on Ta</u>	V= Flow velocity at discharge point (ft/s) R_p = Maximum inside pipe rise (ft) S_p = inside diametere for circular sections of maximum inside pipe span for non-circular sections (ft) T_w = Tailwater depth (ft) Based on Table 11 13 1. A Proformed Scour Hole is used One Half Pipe Pipe Depression (Type I)									
Pin Pan St	ono Sizo:									
	nouted (ft)	Rin Ran Specification	D _{co} Stone Size Requi	red						
0.047		Modified	5 inches							
D:047 Modified Strictes Preformed Scour Hole Dimensions: $F = 0.5(R_p)$ = 0.5 ft C = $3.0(S_p)+6.0(F)$ = 6ft B = $2.0(S_p)+6.0(F)$ = 5ft										
d (Deptł	ו of Stone)	=	12 inches							







Appendix E Water Quality Computations

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023



STORMWATER QUALITY CALCULATIONS Water Quality Volume (WQV)

Basin	Total	Impervious	Percent	Volumetric	WQV	Total Volume	Total Volume
ID	Area (ac.)	Area (ac.)	Impervious	Runoff Coeff., R	(ac-ft)	Required (ac-ft)	Provided ^{1.} (ac-ft)
DET 110	2.31	0.93	40%	0.41	0.079	0.079	0.145

^{1.-} Volume provided below overflow weir

	(1.0 inches) x A x R
wQv –	12

Where:

WQV = Water Quality Volume in acre-feet A = Contributing Area in acres R = 0.05 + 0.009 (I) I = Site Imperviousness as percent

STORMWATER QUALITY CALCULATIONS Water Quality Volume (WQV)

<u>DET 110</u>

Sediment Forebay

Elevation (ft)	Surface Area (ft2)	Volume (ft3)	Volume (ac-ft)	Cumulative Volume (ac-ft)
445.0	291	0.0	0.000	0.000
446.0	518	404.5	0.009	0.009

Main Basin

Elevation (ft)	Surface Area (ft2)	Volume (ft3)	Volume (ac-ft)	Cumulative Volume (ac-ft)
445.0	933	0.0	0.000	0.000
446.0	1,360	1,146.5	0.026	0.026
447.0	2,649	2,004.5	0.046	0.072
448.0	3,665	3,157.0	0.072	0.145

Drawdown Time = 6,316 cf / [(933 sf * 27.4 in/hr)/12] = 2.96 hours

Groundwater Recharge Volume (GRV)

Where: GRV = Groundwater Recharge in cubic feet F = target depth factor per Hydrologic Soil Group in feet

х

I = net increase in impervious area (redevelopment projects)

Т

Analysis Point A	Analysis Point A: (Contains HSG B & HSG C)										
Surface	Existing		Proposed		Difference						
Impv. (HSG B)	32 <i>,</i> 530		40,985		8,455						
Impv. (HSG C)	0		0		0						
Total	32,530		40,985		8,455						
GRV =	0.029	x	8,455	=	245.20						
	0.021	х	0	=	0.00						
					245	CF					
		Total GRV Required		=	245	CF					
		Total GI	RV Provided	=	6,273	CF					

ОК



Appendix F Hydrologic Analysis – Input Computations

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023



	Curve Number C	alcula	ation	S			
Project: Location:	Camp Yankee Trails Site Improvements 343 Plains Road	-		-			
Bv:	Tolland, Connecticut MCB Date: 10/30/23 Cl	_ hecked:			Date:		
Circle one:	Present Developed Wat	ershed:	EXWS	6-10			
Soil Name	Cover Description	С	N Valu	e ^{1.}	Area	Product	
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	CN x Area	
B Soil	Woods - Good Condition	55			38.17	2099.58	
B Soil	Open Space - Good Condition	61			3.92	239.19	
B Soil	Gravel	85			1.62	137.56	
C Soil	Woods - Good Condition	70			1.70	118.66	
N/A	Paved/Impervious	98			0.11	11.22	
N/A	Building	98			0.63	61.97	
N/A	Water	98			0.47	45.99	
			Tota	als = (46.63 0.07285	2714.18 sq mi)	
CN (\	weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{27^2}{46}$	14.18 5.63	• Use	e CN =	58.2]	

₩SLR

	Curve Number C	alcula	ation	s						
Project:	Camp Yankee Trails Site Improvements									
Location:	343 Plains Road	-		_						
	Tolland, Connecticut	_								
By: MCB Date: 10/30/23 Checked: Date:										
Circle one:	Present <u>Developed</u> Wat	ersnea:	PRWS	5-10						
Soil Name	Cover Description	С	N Value	e ^{1.}	Area	Product				
and Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	of CN x Area				
B Soil	Woods - Good Condition	55			35.27	1939.63				
B Soil	Open Space - Good Condition	61			4.75	289.50				
B Soil	Gravel	85			1.43	121.86				
C Soil	Woods - Good Condition	70			1.70	118.66				
N/A	Paved/Impervious	98			0.34	33.35				
N/A	Building	98			0.60	58.86				
N/A	Water	98			0.23	22.66				
L	1	1	I Tota	als =	44.31	2584.52				
				(0.06924	sq mi)				
CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{258}{44}$	34.52 1.31	Use	e CN =	58.3					

	Curve Number Ca	alcula	ation	S						
Project:	Camp Yankee Trails Site Improvements	_								
Location:	343 Plains Road			-						
D. #	Tolland, Connecticut	_ 			Deter					
By: MCB Date: 10/30/23 Checked: Date: Date: Circle one: Present Developed Watershed: PRWS-11										
	Theorem Derenopou	oronou.		,						
Soil Name	Cover Description	CI	N Value	ə ^{1.}	Area	Product				
and Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	Acres Sq. Ft. %	of CN x Area				
B Soil	Woods - Good Condition	55			0.54	29.52				
B Soil	Open Space - Good Condition	61			0.84	51.40				
B Soil	Gravel	85			0.06	51.40				
N/A	Paved/Impervious	98			0.80	5.40				
N/A	Building	98			0.07	78.21				
			Tota	als =	2.31	215.92				
				(0.00361	sq mi)				
CN (י	weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{21}{2}$	5.92 .31	Use	e CN =	93.4					

尜SLR



尜SLR



浆SLR







NOAA Atlas 14, Volume 10, Version 3 Location name: Tolland, Connecticut, USA* Latitude: 41.9274°, Longitude: -72.3121° Elevation: m/ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration				Average	recurrence	e interval (y	vears)				
Duration	1	2	5	10	25	50	100	200	500	1000	
5-min	0.335 (0.255-0.439)	0.402 (0.306-0.527)	0.511 (0.389-0.674)	0.602 (0.455-0.796)	0.727 (0.534-1.00)	0.821 (0.593-1.16)	0.919 (0.646-1.34)	1.03 (0.688-1.53)	1.18 (0.764-1.82)	1.30 (0.826-2.06)	
10-min	0.474 (0.362-0.621)	0.569 (0.434-0.746)	0.724 (0.550-0.953)	0.853 (0.645-1.13)	1.03 (0.756-1.42)	1.16 (0.839-1.64)	1.30 (0.915-1.90)	1.46 (0.974-2.17)	1.67 (1.08-2.58)	1.85 (1.17-2.91)	
15-min	0.558 (0.426-0.731)	0.669 (0.510-0.878)	0.851 (0.647-1.12)	1.00 (0.759-1.33)	1.21 (0.890-1.67)	1.37 (0.986-1.93)	1.53 (1.08-2.23)	1.71 (1.15-2.56)	1.97 (1.27-3.04)	2.18 (1.38-3.42)	
30-min	0.756 (0.577-0.991)	0.908 (0.692-1.19)	1.16 (0.880-1.52)	1.36 (1.03-1.80)	1.64 (1.21-2.27)	1.86 (1.34-2.62)	2.08 (1.46-3.03)	2.33 (1.56-3.47)	2.68 (1.73-4.13)	2.96 (1.87-4.66)	
60-min	0.954 (0.729-1.25)	1.15 (0.874-1.50)	1.46 (1.11-1.92)	1.72 (1.30-2.28)	2.08 (1.53-2.87)	2.35 (1.69-3.30)	2.63 (1.85-3.83)	2.94 (1.97-4.39)	3.38 (2.19-5.22)	3.74 (2.37-5.88)	
2-hr	1.22 (0.934-1.59)	1.46 (1.12-1.90)	1.85 (1.42-2.43)	2.18 (1.66-2.87)	2.63 (1.94-3.62)	2.96 (2.16-4.17)	3.32 (2.36-4.86)	3.74 (2.52-5.56)	4.37 (2.83-6.71)	4.90 (3.11-7.66)	
3-hr	1.40 (1.08-1.82)	1.68 (1.29-2.19)	2.14 (1.64-2.79)	2.52 (1.92-3.30)	3.04 (2.25-4.17)	3.42 (2.50-4.80)	3.84 (2.74-5.61)	4.34 (2.92-6.42)	5.10 (3.31-7.81)	5.76 (3.66-8.98)	
6-hr	1.78 (1.37-2.30)	2.14 (1.65-2.77)	2.74 (2.11-3.56)	3.24 (2.47-4.22)	3.92 (2.92-5.36)	4.42 (3.24-6.19)	4.97 (3.58-7.26)	5.65 (3.81-8.31)	6.70 (4.36-10.2)	7.62 (4.86-11.8)	
12-hr	2.22 (1.72-2.86)	2.71 (2.10-3.48)	3.50 (2.70-4.51)	4.15 (3.19-5.38)	5.05 (3.78-6.88)	5.71 (4.21-7.97)	6.44 (4.66-9.37)	7.34 (4.97-10.7)	8.75 (5.72-13.2)	9.98 (6.38-15.4)	
24-hr	2.64 (2.06-3.38)	3.25 (2.53-4.16)	4.25 (3.29-5.44)	5.07 (3.91-6.54)	6.21 (4.67-8.41)	7.04 (5.22-9.78)	7.96 (5.78-11.5)	9.11 (6.18-13.3)	10.9 (7.15-16.4)	12.5 (8.02-19.1)	
2-day	3.00 (2.34-3.80)	3.72 (2.90-4.72)	4.90 (3.82-6.24)	5.88 (4.55-7.53)	7.23 (5.47-9.75)	8.21 (6.12-11.4)	9.30 (6.80-13.5)	10.7 (7.28-15.5)	12.9 (8.48-19.3)	14.8 (9.56-22.6)	
3-day	3.26 (2.56-4.12)	4.05 (3.17-5.12)	5.33 (4.16-6.77)	6.40 (4.97-8.18)	7.87 (5.97-10.6)	8.94 (6.68-12.3)	10.1 (7.43-14.6)	11.7 (7.95-16.8)	14.1 (9.28-21.0)	16.2 (10.5-24.6)	
4-day	3.49 (2.74-4.41)	4.33 (3.40-5.47)	5.70 (4.46-7.22)	6.84 (5.32-8.71)	8.40 (6.38-11.3)	9.54 (7.14-13.1)	10.8 (7.94-15.5)	12.4 (8.50-17.9)	15.0 (9.90-22.3)	17.3 (11.2-26.2)	
7-day	4.14 (3.27-5.20)	5.09 (4.01-6.40)	6.64 (5.21-8.37)	7.92 (6.18-10.0)	9.69 (7.38-12.9)	11.0 (8.24-15.0)	12.4 (9.13-17.7)	14.2 (9.75-20.4)	17.1 (11.3-25.3)	19.7 (12.7-29.6)	
10-day	4.80 (3.79-6.01)	5.81 (4.58-7.28)	7.45 (5.86-9.37)	8.82 (6.90-11.1)	10.7 (8.16-14.2)	12.1 (9.06-16.4)	13.6 (10.0-19.3)	15.5 (10.6-22.1)	18.5 (12.2-27.2)	21.1 (13.6-31.6)	
20-day	6.87 (5.45-8.55)	7.95 (6.30-9.90)	9.71 (7.67-12.1)	11.2 (8.78-14.0)	13.2 (10.1-17.3)	14.7 (11.0-19.7)	16.3 (11.9-22.6)	18.1 (12.5-25.6)	20.8 (13.9-30.4)	23.0 (15.0-34.3)	
30-day	8.63 (6.86-10.7)	9.73 (7.73-12.1)	11.5 (9.14-14.4)	13.0 (10.3-16.3)	15.1 (11.5-19.6)	16.7 (12.4-22.1)	18.3 (13.2-25.0)	20.0 (13.8-28.1)	22.3 (14.9-32.5)	24.2 (15.8-35.9)	
45-day	10.8 (8.63-13.4)	12.0 (9.52-14.8)	13.8 (11.0-17.1)	15.3 (12.1-19.1)	17.4 (13.3-22.5)	19.1 (14.2-25.0)	20.7 (14.9-27.9)	22.2 (15.5-31.1)	24.2 (16.2-35.1)	25.7 (16.8-37.9)	
60-day	12.7 (10.1-15.6)	13.8 (11.0-17.0)	15.7 (12.5-19.4)	17.2 (13.6-21.5)	19.4 (14.8-24.9)	21.1 (15.7-27.5)	22.7 (16.3-30.4)	24.1 (16.8-33.7)	25.9 (17.4-37.4)	27.1 (17.7-39.9)	

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Back to Top



PDS-based depth-duration-frequency (DDF) curves Latitude: 41.9274°, Longitude: -72.3121°

NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Thu Aug 24 13:10:38 2023

Back to Top

Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

Sample	Sample Round	L (inches)	H1(Inches)	H2(Inches)	t (min)	t (hours)	K (in/hr)	K (ft/day)
	1	3	8	6.00	1	0.017	51.429	102.857
SLR-TP-1	2	3	6.00	4.40	1	0.017	55.385	110.769
	3	3	4.40	3.10	1	0.017	62.400	124.800
	4	3	3.10	1.90	1	0.017	86.400	172.800
	5	3	1.90	0.90	1	0.017	128.571	257.143
	6							
	7							
	8							
	9							
	10							
	11							
	12							
	13							
	14							
	15							
				Sample Ave	rage		76.84	153.67

Sample	Sample Round	L (inches)	H1(Inches)	H2(Inches)	t (min)	t (hours)	K (in/hr)	K (ft/day)
	1	2	8	6.90	1	0.017	17.718	35.436
SLR-TP-2	2	2	6.90	6.00	1	0.017	16.744	33.488
	3	2	6.00	5.00	1	0.017	21.818	43.636
	4	2	5.00	4.25	1	0.017	19.459	38.919
	5	2	4.25	3.50	1	0.017	23.226	46.452
	6	2	3.50	2.75	1	0.017	28.800	57.600
	7	2	2.75	2.25	1	0.017	24.000	48.000
	8	2	2.25	1.50	1	0.017	48.000	96.000
	9	2	1.50	1.00	1	0.017	48.000	96.000
	10	2	1.00	0.50	1	0.017	80.000	160.000
	11							
	12							
	13							
	14							
	15							
		Sample Average 32.78						65.55

(76.84 + 32.78) / 2 = 54.8 in/hr 54.8 in/hr * 50% = 27.4 in/hr



Appendix G Hydrologic Analysis – Computer Model Results

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023


Hydrographs Peak Flowrate Summary (cfs) Existing vs. Proposed

Storm Event	2	yr	10)yr	25	5yr	50)yr	100yr	
Storm Event	Exist	Prop								
Point of Analysis A Peak Flow Rate (cfs)	7.7	7.5	37.0	36.2	61.7	61.7	81.4	81.2	104.6	104.2
Point of Analysis A Peak Runoff Volume (acre-feet)	1.4	1.3	4.6	4.5	7.2	7.0	9.3	9.0	11.8	11.4
DET 110 W.S. Elev. (ft.) Top of Berm Elev. = 450.2	-	447.6	-	448.2	-	448.6	-	448.9	-	449.1
UG 111 W.S. Elev. (ft.) Top of Stone Elev. = 445.0	-	441.5	-	443.4	-	444.0	-	444.2	-	444.7

Study Area

Description

Α

Sweetheart Lake

Watershed Model Schematic



Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd.	Hydrograph	Inflow	Peak Outflow (cfs)					Hydrograph			
NO.	type (origin)	nya(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			7.650			36.97	61.72	81.44	104.55	EXWS-10/A
3	SCS Runoff			7.496			35.61	59.28	78.10	100.14	PRWS-10
4	SCS Runoff			5.736			9.463	11.77	13.44	15.29	PRWS-11
5	Reservoir	4		0.000			3.994	4.732	5.112	6.639	DET 110
6	Reservoir	5		0.000			0.400	2.677	3.179	4.070	UG 111
7	Combine	3, 6		7.496			36.01	61.71	81.15	104.21	10 + 111 / A

2

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description		
1	SCS Runoff	7.650	3	747	1.385				EXWS-10 / A		
3	SCS Runoff	7.496	3	747	1.340				PRWS-10		
4	SCS Runoff	5.736	3	726	0.457				PRWS-11		
5	Reservoir	0.000	3	732	0.000	4	447.58	0.113	DET 110		
6	Reservoir	0.000	3	n/a	0.000	5	441.50	0.000	UG 111		
7	Combine	7.496	3	747	1.340	3, 6			10 + 111 / A		
CY	T-Model02.gp	w			Return P	eriod: 2 Ye	ar	Tuesday, 12 / 19 / 2023			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description
1	SCS Runoff	36.97	3	741	4.625				EXWS-10 / A
3	SCS Runoff	35.61	3	741	4.443				PRWS-10
4	SCS Runoff	9.463	3	726	0.778				PRWS-11
5	Reservoir	3.994	3	732	0.076	4	448.23	0.165	DET 110
6	Reservoir	0.400	3	741	0.005	5	443.41	0.039	UG 111
7	Combine	36.01	3	741	4.447	3, 6			10 + 111 / A
					Return P	Period: 10 Y		Tuesday 1	2/19/2023
CY	T-Model02.gp	W			Return P	eriod: 10 Y	′ear	Tuesday, 12	2 / 19 / 2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description		
1	SCS Runoff	61.72	3	738	7.221				EXWS-10/A		
3	SCS Runoff	59.28	3	738	6.923				PRWS-10		
4	SCS Runoff	11.77	3	726	0.981				PRWS-11		
5	Reservoir	4.732	3	732	0.153	4	448.58	0.197	DET 110		
6	Reservoir	2.677	3	744	0.056	5	444.10	0.053	UG 111		
7	Combine	61.71	3	738	6.979	3, 6			10 + 111 / A		
CY	CYT-Model02.gpw				Return P	eriod: 25 Y	'ear	Tuesday, 12 / 19 / 2023			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	81.44	3	738	9.305				EXWS-10/A	
3	SCS Runoff	78.10	3	738	8.912				PRWS-10	
4	SCS Runoff	13.44	3	726	1.129				PRWS-11	
5	Reservoir	5.112	3	732	0.208	4	448.86	0.223	DET 110	
6	Reservoir	3.179	3	744	0.098	5	444.31	0.057	UG 111	
7	Combine	81.15	3	738	9.009	3, 6			10 + 111 / A	
CY	CYT-Model02.gpw			Return P	eriod: 50 Y	/ear	Tuesday, 12 / 19 / 2023			

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (acft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (acft)	Hydrograph Description	
1	SCS Runoff	104.55	3	738	11.764				EXWS-10/A	
3	SCS Runoff	100.14	3	738	11.258				PRWS-10	
4	SCS Runoff	15.29	3	726	1.294				PRWS-11	
5	Reservoir	6.639	3	732	0.272	4	449.12	0.250	DET 110	
6	Reservoir	4.070	3	738	0.144	5	444.76	0.062	UG 111	
7	Combine	104.21	3	738	11.402	3, 6			10 + 111 / A	
CY	CYT-Model02 apw			Return P	eriod: 100	Year	Tuesday 12/19/2023			

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Pond No. 3 - DET 110

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 445.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	445.00	933	0.000	0.000
1.00	446.00	1,360	0.026	0.026
2.00	447.00	2,649	0.045	0.071
3.00	448.00	3,665	0.072	0.144
4.00	449.00	4,459	0.093	0.237
5.00	450.00	5,310	0.112	0.349

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 14.00	10.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 448.00	449.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	2.60	3.33	3.33
Invert El. (ft)	= 446.50	0.00	0.00	0.00	Weir Type	= 1	Broad		
Length (ft)	= 35.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 8.57	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 27.400 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	445.00	0.00				0.00	0.00			0.000		0.000
1.00	0.026	446.00	0.00				0.00	0.00			0.863		0.863
2.00	0.071	447.00	0.00				0.00	0.00			1.680		1.680
3.00	0.144	448.00	0.00				0.00	0.00			2.325		2.325
4.00	0.237	449.00	5.34 ic				5.34 s	0.00			2.828		8.169
5.00	0.349	450.00	6.55 ic				6.44 s	26.00			3.368		35.81

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Pond No. 1 - UG 111

Pond Data

UG Chambers -Invert elev. = 442.00 ft, Rise x Span = 2.50×4.25 ft, Barrel Len = 7.12 ft, No. Barrels = 36, Slope = 0.00%, Headers = No **Encasement -**Invert elev. = 441.50 ft, Width = 4.25 ft, Height = 3.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (acft)	Total storage (acft)
0.00	441.50	n/a	0.000	0.000
0.35	441.85	n/a	0.004	0.004
0.70	442.20	n/a	0.007	0.010
1.05	442.55	n/a	0.009	0.019
1.40	442.90	n/a	0.009	0.027
1.75	443.25	n/a	0.008	0.035
2.10	443.60	n/a	0.008	0.043
2.45	443.95	n/a	0.007	0.050
2.80	444.30	n/a	0.006	0.057
3.15	444.65	n/a	0.004	0.061
3.50	445.00	n/a	0.004	0.064

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 443.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 40.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 5.00	0.00	0.00	n/a	-				
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 27.400 (1	oy Wet area	a)	
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00	-		

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

-	-	-											
Stage ft	Storage acft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0.000	441.50	0.00								0.000		0.000
0.35	0.004	441.85	0.00								0.805		0.805
0.70	0.010	442.20	0.00								0.919		0.919
1.05	0.019	442.55	0.00								1.032		1.032
1.40	0.027	442.90	0.00								1.146		1.146
1.75	0.035	443.25	0.26 ic								1.260		1.522
2.10	0.043	443.60	1.30 ic								1.374		2.673
2.45	0.050	443.95	2.56 ic								1.488		4.045
2.80	0.057	444.30	3.38 ic								1.601		4.983
3.15	0.061	444.65	4.05 ic								1.715		5.770
3.50	0.064	445.00	4.63 ic								1.829		6.460



Appendix H Operation and Maintenance Manual

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023



尜SLR

Camp Yankee Trails Site Improvements

343 Plains Road Tolland, Connecticut

Stormwater Operations and Maintenance Manual

Prepared for: Girl Scouts of Connecticut

20 Washington Avenue North Haven, CT 06473

Prepared by:

SLR International Corporation

99 Realty Drive, Cheshire, Connecticut, 06410

SLR Project No.: 141.13280.00006

December 20, 2023

Making Sustainability Happen

Stormwater Operations and Maintenance Manual

Camp Yankee Trails Site Improvements 343 Plains Road Tolland, Connecticut SLR #141.13280.000006

1.0 Introduction

After construction is completed, stormwater systems on the property will need to be periodically maintained. The stormwater system consists of storm drainage piping, catch basin, yard drain and manhole structures, underground chambers, and a stormwater detention basin. In order to ensure optimal performance of the system, the following stormwater maintenance program has been established. This manual provides an outline of the operation procedures but may be adjusted based upon specific site conditions.

A representative of Girl Scouts of Connecticut or designee will be responsible for the maintenance of stormwater control structures. The name and contact information of this representative are to be determined.

2.0 Storm System Elements

2.1 Stormwater Infiltration Basin

The stormwater infiltration basin should be maintained so that the system can effectively treat contributing stormwater runoff.

- 1. The stormwater infiltration basin shall be cleaned of debris and sediment upon the completion of construction.
- 2. The stormwater infiltration basin shall be inspected during spring cleanup and again just prior to the winter season. All dead plants and missing mulch shall be replaced, and any necessary pruning of vegetation shall be completed.
- 3. The surface of the stormwater infiltration basin shall be inspected on a quarterly basis after the first 6 months of successful operation and after heavy runoff events (i.e., >3.0" in a 24-hour period). One inspection shall occur immediately following the completion of winter sanding and sweeping operations, and one shall occur just prior to the winter season. Any accumulated debris and sediment shall be removed.

2.2 Parking Areas

The parking area shall be swept annually. Sweeping should occur in the spring between April 15 and May 15 after winter sanding.

2.3 Catch Basins (Inlets)

Drain inlets are designed with 2-foot minimum depth sumps for collecting coarse sediment. All inlets should be inspected two times per year, typically when the site is swept in the spring after winter sanding and in the fall after all the leaves have fallen.



Sediment should be removed when it extends to within 6 inches of the outlet pipe invert or not less than once per year. Cleanout with a vacuum truck is generally the best and most convenient method. The sediment shall be disposed of in an approved offsite location in accordance with town and state requirements.

2.4 Lawn and Vegetated Areas

Vegetated cover shall be maintained on all earth surfaces to minimize soil erosion. Use of fertilizer should be avoided. If fertilizers are deemed necessary they should be minimized to the greatest extent possible and should be applied with prudent application methods.

2.5 Underground Chamber Systems

The underground chamber system shall be completely cleaned of accumulated debris and sediment upon completion of construction. For the first year after construction is completed, the underground chamber system shall be inspected on a quarterly basis. Any accumulated debris shall be removed, and any repairs shall be made to the units, as required. From the second year onward, visually inspect the underground chamber system twice per year, once in the spring and once in the fall after the fall cleanup of leaves. Complete any additional maintenance required per the manufacturer's specifications.

3.0 Inspection Procedures

Inventory sheets shall be created to note any noncompliance during each inspection. Fill out notes according to the attached requirements of each structure noting shortcomings, problems, and required maintenance on each. The inventory sheets shall include the following:

- 1. Date of inspection
- 2. Name of inspector
- 3. Underground drainage structures/cleanouts
- 4. Sediment load
- 5. Any other item that could affect the proper function of the facility

13280.00006.d1923.rpt.docx



Making Sustainability Happen



Appendix I Watershed Maps

Camp Yankee Trails Site Improvements

343 Plains Road, Tolland, Connecticut

Drainage Report

Prepared for: Girl Scouts of Connecticut

SLR Project No.: 141.13280.00006.0060

November 20, 2023

Revised December 20, 2023







wing: W:\CADEESIGN\13280.0006--DE\CAD\CYT-HYDROO1.bWG Layout Tab:PRWS htted by: MBERARDI On this date: Tue, 2023 December 19 - 2:16pm





Making Sustainability Happen

wing: W:\CADDESIGN\13280.00006-DE\CAD\CYT- GRADING.DWG Layout Tab:GR-2 tted by: MBERARDI On this date: Wed, 2023 December 20 - 2:15pm



MATCHLINE - SEE SHEET GR-3 \sim Jel -1.5:1 RIP RAP SLOPE (460) 1.5:1 RIP RAP SLOPE 1.5... STORMWATER WATER -UNDERGROUND STORMWATER WATER INFILTRATION SYSTEM OCS 110_____ FES 5 INV.=445.0 Ann X X X 442 ⊴× ⊲OHW57 FES 1_/ INV.=441.0 X 437.9 GR-4, ENLARGEMENT STORMWATER DETENTION OUTLET – REFER TO UTILITY PLANS







Copyright SLR International Corporation - 2021











SEDIMENT & EROSION CONTROL SPECIFICATIONS

GENERAL:

- VERTICAL (2:1).
- VERTICAL (2:1).

- SITE

- GROWTH OF PLANTS.
- DIAMETER), LUMPS OF SOIL, ROOTS, TREE LIMBS, TRASH, OR CONSTRUCTION DEBRIS. IT SHOULD BE FREE OF ROOTS OR RHIZOMES SUCH AS THISTLE, NUTGRASS, AND QUACKGRASS.

SPREAD TOPSOIL UNIFORMLY TO A DEPTH OF AT LEAST SIX INCHES (6"), OR TO THE DEPTH SHOWN ON THE

TEMPORARY VEGETATIVE COVER SHALL BE ESTABLISHED ON ALL UNPROTECTED AREAS THAT PRODUCE SEDIMENT, AREAS WHERE FINAL GRADING HAS BEEN COMPLETED, AND AREAS WHERE THE ESTIMATED APPLIED IF AREAS WILL NOT BE PERMANENTLY SEEDED BY SEPTEMBER 1.

- PER 1,000 SQ. FT.) AND SECOND APPLICATION OF 200 LBS. OF 10-10-10- (5 LBS. PER 1,000 SQ. FT.) WHEN GRASS IS FOUR INCHES (4") TO SIX INCHES (6") HIGH. APPLY ONLY WHEN GRASS IS DRY.
- SLOPING.

COVER RYEGRASS SEEDS WITH NOT MORE THAN 1/4 INCH OF SOIL USING SUITABLE EQUIPMENT. 4. MULCH IMMEDIATELY AFTER SEEDING IF REQUIRED. (SEE VEGETATIVE COVER SELECTION & MULCHING SPECIFICATION BELOW.) APPLY STRAW OR HAY MULCH AND ANCHOR TO SLOPES GREATER THAN 3% OR WHERE CONCENTRATED FLOW WILL OCCUR.



GENERAL:

PERMANENT COVER IS NEEDED.

- 5. APPLY TOPSOIL AS INDICATED ELSEWHERE HEREIN.

TEMPORARY VEGETATIVE COVER

- (EXCEPT WHEN HYDROSEEDING).

- (EXCEPT WHEN HYDROSEEDING).

- TOWARD THE PREVIOUSLY LAID BALE TO FORCE BALES TOGETHER.
- SHALL OVERLAP A MINIMUM OF TWO FEET (2').

- CONSTRUCTION



NCE INTER	RVALS		
NCE	FAILURE INDICATORS	REMOVAL	
ND OF A STORM WITH A LEAST 0.5 FEET BELOW UMULATION REACHES ½	- TURBID WATER - EXCESSIVE SEDIMENT ACCUMULATION - OVERTOPPING EVIDENCE	TST MAY BE REMOVED ONCE THE CONTRIBUTING DRAINAGE AREA IS PERMANENTLY STABILIZED.	
ND OF A STORM WITH A T BE REMOVED ONCE ITS DURING PUMPING	- PHYSICAL DAMAGE OR DECOMPOSITION - EVIDENCE OF OVERTOPPED OR UNDERCUT FENCE - EVIDENCE OF SIGNIFICANT FLOWS EVADING CAPTURE - REPETITIVE FAILURE	SILT FENCE MAY BE REMOVED AFTER UPHILL AND SENSITIVE AREAS HAVE BEEN PERMANENTLY STABILIZED.	
ND OF A STORM WITH A F BE REMOVED ONCE THE ISPECT FREQUENTLY IONS.	 PHYSICAL DAMAGE OR DECOMPOSITION EVIDENCE OF OVERTOPPED OR UNDERCUT FENCE EVIDENCE OF SIGNIFICANT FLOWS EVADING CAPTURE REPETITIVE FAILURE 	HAY BALES MAY BE REMOVED AFTER UPHILL AREAS HAVE BEEN PERMANENTLY STABILIZED.	
CTION ACTIVITIES, R DAMAGES. OTHERWISE ND OF A STORM WITH A JRE AND ANY OTHER	- PHYSICAL DAMAGE - EXCESSIVE SCOURING/EROSION - REPETITIVE FAILURE	TEMPORARY DIVERSIONS MAY BE REMOVED ONCE CONSTRUCTION HAS CEASED AND THE CONTRIBUTING DRAINAGE AREA HAS BEEN PERMANENTLY STABILIZED.	PRIVE TING.COM
SIN CONTAINS MORE ROUNDING SILT FENCE	- RIPPED BAG - FAILED HAY BALES / SILT FENCE - SIGNIFICANT SILT PRESENCE IN STORM DRAINAGE SYSTEM OUTFLOW.	INLET PROTECTION MAY BE REMOVED ONCE THE SITE HAS BEEN PERMANENTLY STABILIZED, AND ALL SECTIONS OF ROADWAY HAVE BEEN PERMANENTLY PAVED.	99 REALTY E CHESHIRE, C 203.271.177 SLRCONSUL
ATELY REPAIR DAMAGES. ALES MAY BE	 EVIDENCE OF STOCK PILE DIMINISHING DUE TO RAIN EVENTS FAILURE OF SILT FENCE 	STOCKPILE PROTECTION MAY BE REMOVED ONCE THE STOCKPILE IS USED OR REMOVED.	
PROPEX SILT STOP T CONTROL FABRIC C D EQUAL (GEOTEXTIL	DR LE) STABILIZE ENTIRE PILE WITH VEGETATION OR COVE	R 2 1 SLOPE OR LESS	DESCRIPTION DATE OWC COMMENTS 12/20/2023
O OF GEOTEXTILE NTO SOIL	1. AREA CHOSEN FOR STO	STRAWBALES OR SILTFENCE MIN. SLOPE INSTALLATION NOTES	
NNEL	STRAP	<section-header></section-header>	EDIMENT & EROSION CONTROL NOTES & DETAILS AMP YANKEE TRAILS ITE IMPROVEMENTS 3 PLAINS ROAD 3. PLAINS ROAD DLLAND, CONNECTICUT
WIDTH= W DEPTH= D	Section A-A roadway surface Section A-A 3.5 2% slo Section of water bottom of water bar channel Section A-A	S'or 6 max. ppe	の I ひ の え 子 SMM SMM MTD DESIGNED DRAWN CHECKED AS NOTED SCALE NOVEMBER 21, 2023 DATE 141.13280.00006 PROJECT NO. 20 OF 26 SHEET NO.
ROL DEVIC	<u>E</u> (5.78) <u>W</u>	2002 Connecticut Guidelines for Soil Erosion and Sediment Control ATER BAR (WB) NOT TO SCALE	SE-3



A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)

) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY

A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED



PERIMETER STONE EXCAVATION WALL (CAN BE SLOPED OR VERTICAL)

NOTES:

С

PLEASE NOTE

ABOVE

- CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS. 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
- TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS. • TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2". COLORS

STORMTECH SC-740 CHAMBERS





-740	TEC	HNIC	JAL	SPE	CIFI	CAT	ION
///////////////////////////////////////	///////////////////////////////////////	///////////////////////////////////////	7/7//7777///	/T//////T////	/7//7///////	///////////////////////////////////////	·//T//7//7/





1. MATERIALS

SIEVE SIZE	BY WEI
3 INCH	100
NO. 4	60-95
NO. 10	50-95
NO. 40	30 - 75
NO. 100	20 - 65
NO. 200	10-40

3. PLACEMENT



Engineering Review

December 21, 2023

Inland Wetlands & Watercourses Commission Town of Tolland c/o Michael D'Amato, Interim Wetlands Agent 21 Tolland Green Tolland, CT 06084 Via email

RE: 343 Plains Road, Camp Yankee Trails Site Improvements IWC 23-6 Engineering Review

Commission Members:

As requested, CHA reviewed the following materials for stormwater and general engineering standards that may impact the regulated area:

ltem 1	Eight (8) revised plan sheets entitled "Camp Yankee Trails Site Improvements, 343 Plains Road, Tolland, Connecticut", sheets GR-2, GR-4, UT-2, SE-1, SE-2, SE-3, SD-4, and SD-5, prepared for Girl Scouts of America, prepared by SLR, dated November 21, 2023, revised December 20, 2023
Item 2	Drainage Report, Camp Yankee Trails Site Improvements, 343 Plains Road, Tolland, Connecticut, prepared by SLR, dated November 20, 2023, revised December 20, 2023
Item 3	Tolland Inland Wetlands & Watercourses Commission Comment Response Letter, addressed to Michael D'Amato, prepared by SLR, dated December 20, 2023
ltem 4	CHA Comment Response Letter, addressed to Chuck Eaton, prepared by SLR, dated December 20, 2023

CHA offers the following comments based on the Tolland LID and Stormwater Management Design Manual, 2004 Connecticut Stormwater Quality Manual, and general engineering practice:

CHA's previous review comments are included below in normal text. Updates to those comments are included in *italics*. Any new comments, based on the revised application materials, are included in **bold** text.

- 1. CHA recommends the Designer provide rational for meeting the State or Tolland stormwater standards. The Drainage Report appears to only discuss water quality and quantity treatment. *The Designer revised the Drainage Report to include additional stormwater standards. This comment is addressed.*
- It appears infiltration tests were performed for the stormwater basins; however, no information other than the infiltration testing rates is provided. A narrative, type of test performed, and testing locations must be provided.
 Information regarding the infiltration testing was provided in the response to comment letter; however, it should be added to the Drainage Report for the Town's record and documentation.
- 3. Test pits are required for properly siting and designing the stormwater basins. This will provide required design information on soil types, depth to ledge and depth to groundwater. Test pit locations and logs must be provided. Based on soil mapping it appears the proposed stormwater basins are located within a type B soil; however, the very high infiltration rates obtained by the infiltration testing are not typical of a type B soil. Test pits must be provided to validate and determine the soil types.

Test pit locations and log information have been added to the plans. A test pit is required prior to construction for Detention System 111 to verify the depth to high groundwater or ledge. The current test pits only extend 0.8-feet below the bottom of the system. Test pits must be provided to ensure the systems are designed pursuant to the Connecticut Stormwater Quality Manual. A note requiring this must be added to the plans and the results provided to the Town prior to construction.

- Design and siting rational must be provided for Stormwater Basins 110 and 111 based on test pits. See Comment No. 3. Design pursuant the Tolland LID Manual or the Connecticut Stormwater Quality Manual must be provided and fully described. Calculations and descriptions such as drawdown time, depth to high groundwater, pretreatment, etc. must be provided. *Provided. See Comment No. 3. This comment is addressed.*
- Pretreatment is required for Stormwater Basin 110. CHA recommends a forebay within Stormwater Basin 110.
 Provided. This comment is addressed.
- 6. Although the infiltration testing supports an infiltration rate of 27.4 inches per hour, the rate will be limited by the surface soil. It does not appear that a cross section of the basin or a call out for the type of soil that will line the basin is provided. CHA recommends an engineered soil consisting of sand, loam, and compost. Typically this engineered soil provides an infiltration rate of 2.41 inches per hour. This rate would then be used as the infiltration rate in the drainage calculations for Stormwater Basin 110.

The Designer revised the bottom design and provided a cross section of Stormwater Basin 110. The revised design will allow the use of the 27.4 inches per hour infiltration rate. This comment is addressed.



7. Drainage calculations for Stormwater Basin 110 use a weir elevation of 448.4. The elevation called for on the plans is 449.4. The calculations, results, and associated narrative must be revised accordingly.

The Designer revised the elevations for Stormwater Basin 110; however, the following discrepancies still exist:

- Emergency weir elevation: plan 449.2, calculations 449.0
- Overflow grate elevation: Plan Sheet GR-2 449.4, correct elevation 448.0
- Stormwater Basin 110 Infiltration Stone Detail: Sheet SD-5 Bottom Elev 448.0, correct elevation 445.0
- 8. The provided water quality volume based on the drainage calculations appears to be 0.156 acrefeet. The water quality chart on page 35 of the PDF indicates 0.195 acre-feet. This chart must be updated or an explanation of how the provided water quality volume was achieved must be provided.

Provided. The correct water quality volume provided of 0.145 acre-feet is shown in the revised Drainage Report. This comment is addressed.

9. No calculations or cross sections are provided for the "vegetated swale" on the eastern side of the proposed access road to the waterfront improvements. It is unclear if the proposed swale can properly convey runoff to the stormwater basins without impacting the waterfront area or Sweetheart Lake.

Calculations are provided indicating the vegetated swale will not overtop through a 25-year storm event; however, it is unclear if the proposed vegetation can sustain the proposed velocity of stormwater runoff without the swale eroding. Calculations must be provided indicating the vegetated swale will be stable through the design storm event.

- Proposed riprap is called out as both 1.5:1 and 1:1 slopes on the plan set. This call out must be consistent within the plan set.
 The revised plans call for 1.5:1. This comment is addressed.
- 11. Inspection ports for Stormwater Basin 111 must be labeled on the plan set. *Provided. This comment is addressed.*
- 12. Information must be provided for the beach sand construction at the waterfront improvement area. It is unclear how this area will be modified and how this may impact Sweetheart Lake. *The Designer provided an explanation of the beach sand construction in the response letter and added a cross section of the area in the revised plans. CHA suggests providing a callout or detail on the plans indicating the materials for the sand beach (similar to the response letter description) if that method and/or material is acceptable to the Commission. Currently the plans only callout for "sand beach".*
- 13. CHA recommends sediment barrier be installed at the toe of slope (around the bottom) of Stormwater Basin 110 to prevent fines from reducing the infiltration capacity of the basin while the side slopes are being stabilized.

Provided; however, with the addition of the "stone wick" in the bottom of Stormwater Basin 110, CHA recommends also installing sediment barrier at the edge of the wick to prevent topsoil



from the bottom of the basin from entering the wick and clogging the infiltration system during the stabilization period.

14. A sequencing plan must be provided for the construction and associated sediment and erosion control of the stormwater basins. The basins cannot be used as temporary sediment basins due to the reduction of infiltration from eroded construction fines. CHA recommends the use of a separately located temporary sediment trap to allow the construction of the stormwater basins once the upgradient site is fully stabilized.

The Temporary Dewatering Underdrain for Temporary Sediment Traps Detail on Sheet SE-3 indicates the underdrain will be connected to an existing catch basin. This callout must be clarified as it does not appear there are existing catch basins within the vicinity of the temporary sediment trap. Otherwise, this comment is addressed.

- 15. A long-term stormwater operation and maintenance plan must be provided to ensure the stormwater management systems continue to function as designed. The location of the systems upgradient and adjacent to Sweetheart Lake make the implementation of this plan important to prevent stormwater system failures that will directly impact the Lake. The proposed vegetated swale, and stone infiltration strips/islands must be added to the long-term stormwater operation and maintenance plan.
- 16. The Preformed Scour Hole Detail on Sheet SD-5 must be updated to correctly identify FES 5. *Provided. This comment is addressed.*

Please contact me if you have any questions regarding these comments.

Sincerely,

Chuck Eaton, P.E., LEEP-AP

Tolland Town Engineer

v:\projects\ehct105\projects\muni_ct\tolland\2019400.000_tolland_generalservices\application reviews\343 plains road\2023-12-21 engineering review - 343 plains rd.docx

